



Engineering Assessment Report

Application at Church Fields East, Mulhuddart, Dublin 15.

May 2023

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This document has been prepared and checked in accordance with Waterman Group's IMS (BS EN ISO 9001: 2015, BS EN ISO 14001: 2015)

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Comments



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1. Introduction

1.1 Context

This Engineering Assessment Report (EAR) has been prepared by Waterman Moylan as part of the documentation in support of the Church Fields East development planning application for a proposed residential development at Damastown Avenue, Mulhuddart, Dublin 15.

This report assesses wastewater and surface water drainage, water supply infrastructure and the road and transportation network in the vicinity of the site, and details the criteria used to design the proposed wastewater and surface water drainage, water supply and transport networks.

1.2 Site & Proposed Development Description

The proposed development relates to a site of c.5.52 hectares at Church Fields East, Mulhuddart, Dublin 15. The development site is located south of Damastown Avenue; west of Church Road; east of previously permitted residential development at Church Fields (Planning Reg. Ref.: PARTXI/012/21); and north of a permitted linear park (Eastern Linear Park Planning Reg. Ref.: PARTXI/012/21), in the townland of Tyrrelstown, Dublin 15. The proposed development seeks the construction of 217 no. residential units (ranging from 2 – 4 storeys in height) in a mixed tenure development, comprising of 121 no. houses and 96 no. apartments. The development will also include the provision of car parking, cycle parking, new pedestrian / cycle links, services, drainage and attenuation, and all associated site and infrastructural works.

Refer to Figure 1 for the location of the proposed development. Refer to Waterman Moylan Drawing 20-074-P4010 for details.

The proposed development consists of:

- 217 Residential units (121 houses, 96 apartments)
- The provision of access roads and associated infrastructure
- SuDS features such as swales, permeable paving, green roofs, and rain garden planters.
- Upgrading 2No. attenuation systems in the Church Fields Housing and Eastern Linear Park



Figure 1: Site Location (image taken from Google Earth)

The site falls from northeast to southwest at a natural slope of c. 1:54, ranging in levels from 87.00m to 80.00m OD Malin. Vehicular access to the site is via the Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21) lands to the west. The Church Fields Link Road and cycle network (currently under construction) services the entire Church Fields lands by linking Ladyswell Road to the south and Damastown Avenue to the north.



Figure 2: Church Fields Site Strategy (image taken from Google Earth)

The subject site is zoned as "RS" by the local authority and is deemed appropriate for the provision of residential development and to protect and improve residential amenities as set out in the Fingal Development Plan 2023-2029.

Figure 3: Fingal County Council Zoning



1.3 Background of Report and Summary

This report describes the criteria used to design and detail the options available for the disposal of stormwater (subject to a restriction to the discharge rate), disposal of wastewater, water supply and the road layout for the proposed development. The proposed development consists of 217 No. units which consists of a mixture of residential houses and apartments.

1.3.1 Wastewater

It is proposed that the foul water from the overall Church Fields development will drain via gravity in a southwesterly direction and discharge into the existing Ø900mm foul water trunk sewer located along the western boundary, approximately 800m from the subject site. The Ø900mm trunk sewer conveys the foul water in a southerly direction and ultimately to Ringsend WWTW.

1.3.2 Surface Water

It is proposed that the surface water requirements will be served by a network of gravity pipes ranging in size from Ø225mm to Ø525mm diameter. The drainage catchment that will outfall at a restricted rate equal to 3.70 l/s/Ha. The subject site has its own attenuation system, consisting of an above ground detention basin combined with a supplementary below ground cellular stone storage area.

The surface water from the subject site will outfall into the Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21) drainage network to the west of the site. Church Fields Housing and Eastern Linear Park Development drains westwards ultimately outfalling at the

southwestern corner of the overall Church Fields lands via the existing infrastructure provided by the external roads project and outfall through their network into the River Pinkeen.

1.3.3 Water Supply

Currently, there is an existing Ø300mm diameter watermain traversing the subject site from the southwest towards the northeast of the site. Irish Water have granted a diversion application for this watermain, under DIV22229. The diverted watermain will run along Damastown Avenue to the north and then south along the new Church Fields link road. A new watermain layout will be constructed for Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21) which will be fed from the Church Fields link road. The subject site will connect into the Church Fields Housing and Eastern Linear Park Development network.

Figure 4: Existing Services



1.3.4 Flood Risk Assessment

A site-specific Flood Risk Assessment has been carried out for the proposed development and accompanies this submission under separate cover. The report assesses the flood risks at the site considering; coastal, fluvial, pluvial, groundwater, and for human/ mechanical error. The site is classified as Flood Zone C and the overall risk of flooding is deemed to be low.

2. Wastewater Network

2.1 Existing Wastewater Network

It is proposed that the foul water from the Church Fields development will drain by gravity in a southwestern direction and discharge into the existing Ø900mm foul water trunk sewer located along the western boundary via a single outfall. The entire Church Fields lands will be served by a Ø300mm diameter trunk sewer, that branches off into each of the development areas. All of these areas will be served by Ø150mm to Ø300mm diameter pipes in line with the Irish Water requirements.

The impact of the foul flow based on the entire Church Fields lands (c. 1,000 No. units) on the Irish Water network was assessed following the submission of a pre-connection enquiry form issued to Irish Water. A Confirmation of Feasibility has been issued by Irish Water on the 18th of April 2023 which confirms capacity for the subject site in the surrounding network. Please refer to Appendix A for the details.

2.2 Wastewater Network Design

Drains generally will consist of PVC pipes (to IS 123) and all foul water sewers within the development will be laid to comply with the requirement of the Building Regulations and in accordance with the recommendations contained in the Technical Guidance Documents, Section H.

Wastewater sewers which will be taken into charge will be laid strictly in accordance with Irish Water's requirements for taking in charge. In accordance with the Irish Water "Code of Practice for Wastewater Supply", Ø150mm nominal internal diameter sewers have been proposed for carrying wastewater from 20 properties or less: whilst Ø225mm nominal internal diameter carrying Wastewater from more than 20 properties. Furthermore, where there are at least ten dwelling units connected, the Ø150mm diameter pipes are laid at a minimum gradient of 1:60 for up to nine connected dwelling units. All manholes will be watertight to prevent groundwater ingress into the foul drainage system. Construction details for the proposed drainage systems are included in the accompanying planning submission drawings.

As part of this planning application, we have submitted the wastewater & watermains design to Irish Water for design vetting. A statement of design acceptance was issued, please refer to Appendix C.

2.3 Wastewater Calculations

The wastewater drainage for the proposed development has been designed so that minimum cleansing velocities outlined in the "Irish Water Code of Practice for Wastewater Infrastructure" are achieved for all foul sewers. The peak foul flow is based on Irish Water recommended peak demand/flow factors which are provided in the Irish Water 'Code of Practice for Wastewater Infrastructure', Wastewater Flow Rates for Design. Pipe capacities and velocities have been calculated using Colebrook-White formula with a roughness coefficient (Ks) of 1.5mm.

As per the Code of Practice, the domestic wastewater loads have been calculated based on 2.7 persons per unit with a per capita foul flow of 150 litres per head per day. Based on the Irish Waters Code of Practice, the peak foul flow from the subject site will be as follows:

Table 1: Calculation of approved Foul Water Flow

		Flow	Population per Unit		Total
Description	No. of Units /	l/h/day	/ Floor Area	Factor	Discharge
					(l/d)
Apartment Units	96	150	2.7	1.1	42,768
Housing Units	121	150	2.7	1.1	53,906
				Total	96,674 I/d

Table 2: Calculation of Proposed Foul Water Flow

96,674	l/d
1.119	l/s
6.713	l/s
	1.119 6.713

The total dry weather flow from the development is 1.119 l/s, with a peak flow of 6.713 l/s. A peak foul flow factor of 6 has been used, as per the Irish Water Wastewater Code of Practice.

* Domestic Wastewater Peaking Factors: For the design of new or upgraded wastewater networks, the peaking factors applied to domestic wastewater flows (PfDom) are to be in accordance with the Figure 5 below.

Figure 5: Peaking Factor Design for Wastewater, Section 2.2.5 IW Wastewater Code of Practice

Population	Peaking Factor (Pf _{Dom)}
0 to 750	6
751 to 1,000	4.5
1001 to 5,000	3.0
5,001 to 10,000	2.5

As shown in the table above the peak flow from the proposed foul network will be 6.713 l /s. The proposed foul network is designed with a minimum gradient at a range as set out in the Irish Water Code of Practise.

The outfall pipe from the development is a Ø300mm pipe laid at a minimum gradient of 1:200 which has sufficient capacity to serve all of the future development on the Church Fields lands, and outfall into the existing 900mm diameter infrastructure located approximately 800m to the west of the site. Therefore, there is adequate capacity in the public foul sewer available to cater for the proposed development. The proposed foul network has been designed with Causeway Flow software and will discharge via gravity. Please see Appendix B for details of the foul water design calculations.

3. Surface Water Drainage

3.1 Introduction

The greenfield runoff rate of the site has been calculated using the Institute of Hydrology report No 124 "Flood Estimation for Small Catchments". The subject site's runoff will be restricted to the equivalent of the Qbar runoff rate of 3.70 l/s as agreed with Fingal County Council's drainage department in discussions as part of finalising the overall site strategy for the Church Fields lands.

Surface water runoff shall be restricted via a Hydro-Brake, or similar approved, installed at the outfall manhole of the surface water catchment with excess stormwater attenuated within the development site.

The proposed surface water drainage system for this development will be designed as a sustainable urban drainage system and will use above and below ground attenuation together with a flow control device, grass swales, green roofs, rain garden planters, filter drains, and permeable paving to:

- Treat runoff and remove pollutants to improve quality.
- Restrict outflow and control the quantity.
- Increase amenity value.

Strict separation of surface water and wastewater will be implemented within the development. Drains will be laid out to minimise the risk of inadvertent connection of waste pipes etc. to the surface water system. Excess stormwater shall be attenuated within the 800mm deep detention basin and below ground stone tank system.

Surface water should be managed in accordance with council specific prerequisites and with the Greater Dublin Strategic Drainage Study (GDSDS) Regional Drainage Policies Volume 2, for New Developments and CIRIA documents. These documents specify that surface water run-off should be managed as close to its source as possible, with the re-use of rainwater within the buildings prioritised.

Surface water local drains will be Ø150 mm to Ø225 mm and generally will consist of PVC (to IS 123) or concrete socket and spigot pipes (to IS 6). These drains will be laid to comply with the Requirement of the Building Regulations 2010, and in accordance with the recommendations contained in the Technical Guidance Documents, Section H. Surface water public sewers will be Ø225 mm to Ø525 mm and generally will consist of PVC or concrete socket and spigot pipes (to IS 6) and will be laid strictly in accordance with the requirements of Fingal County Council.

3.2 Surface Water – Existing

The subject site is bounded by Damastown Avenue to the north, by Church Road to the east, the proposed linear park bounds the site to the south, Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21) of the Church Fields lands bound the site to the west. The river Pinkeen is located further west along the boundary of Church Fields West of the Church Fields lands.

The existing record drawings for the area surrounding the subject site were obtained from a GPR survey conducted by CSS Land Surveys in September 2020. The existing records drawings show that there is an existing Ø225mm diameter surface water sewer used to discharge surface water from the Avondale Park development to a dry ditch via a headwall at a rate of 4.38 l/s, located adjacent the southwestern boundary

of the Church Fields lands, approximately 800m from the subject site. The dry ditch continues further southwest and ultimately discharges to River Pinkeen. It is not required to be diverted.



Figure 6: Watercourses in Close Proximity to the Site

As part of the Church Field Link Road works contract, it is proposed to install a Ø750mm diameter pipe which will serve the development, as well as the road upgrade. The surface water is proposed to outfall and flow through 3 No. detention basins, located in the southwestern corner of the overall Church Fields Site Strategic development. It will be constructed as part of the roadworks contract, with an outfall into the dry ditch to the west of the Church Fields site which ultimately traverses to the river Pinkeen.

3.3 Site Characteristics

The site characteristics are specified in the following sections.

Soil type 2 has been used for attenuation calculations below. Additionally, see the extract from Soil Map of Ireland below with Site Location shown:

Figure 7: Soil Map of Ireland extract



Table 3: Site Characteristics

SAAR	815 mm
Soil Index	Soil Type 2 = 0.3
Climate Change	20 %
Qbar / Hectare	3.70 l/s/Hectare*

* It has been agreed with Fingal County Council in pre-application meetings that the allowable outfall for the Church Fields Site Strategic Plan area is 3.70 l/s/Ha.

3.3.1 Drainage Catchment

It is proposed to attenuate the surface water run off for the catchment in the open space at the centre of the subject site. Due to the topography of the site, it is not possible to attenuate the full area within the open space. The western boundary of the site will connect into the surface water network for Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21), into catchments A3 & A4. A design capacity check was completed on the granted attenuation systems.

We have liaised with Mr Daragh Sheedy (Executive Engineer FCC) and a design capacity check was completed on the granted attenuation systems. We have agreed to upgrade the capacities of the attenuation systems A3 & A4 using cellular storage systems (Stormtech or similar approved) to cater for the additional flows. We note that the previously granted overground detention basin at A3 will be unchanged and remain the same. Attenuation A4 is solely an underground storage system, the proposed cellular storage tank will have a smaller footprint than was previously granted.

Please refer to Appendix G for capacity checks and drawings 20-074-P4202 & 4203 for details. The catchment and hardstanding areas are indicated in the figure below:

	Catchment Area (m ²)	Impermeable Area (m ²)	% Hardstanding
Catchment 4A	45,408	18,163	40 %
Catchment A3 (Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21))	23,582	11,908	51 %
Catchment A4 (Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21))	25,123	12,723	51 %

Table 4: Catchment Attributes

Figure 8: Drainage Catchment Areas



3.4 Outflow Limits

It has been agreed with Fingal County Council to have an allowable outfall of 3.7 I/s/Ha as part of the initial development of the Site Strategic Plan layout for the Church Fields development. Each catchment of the overall lands is proposed to be restricted by a Hydro-Brake, or similar flow control device approved, which will be located immediately upstream of the catchment outfall. The outfall from the subject site is calculated to be 16.8 I/s and will be achieved by means of a Hydro-Brake. The allowable outflow for the entire Church Fields lands is calculated as 35.01 I/s whereafter the surface water will outflow into the river Pinkeen via the 3 No. Detention Basins built as part of the Church Field Link Road works under a separate contract.

3.5 Surface Water – Proposed

The proposed development will ultimately outfall into the Pinkeen River to the far west of the site at an overall allowable outfall rate of 35.01 l/s. Surface water runoff shall be restricted via a Hydro-Brake, or

similar approved, installed at the outfall manhole of the surface water catchment with excess stormwater attenuated within the development site.

As part of this planning application a site Investigation has been conducted by Ground Investigations Ireland and indicated that the proposed site does not have adequate percolation, therefore it is proposed that a combination of above-and-below ground storage within each catchment. A shallow above-ground detention basin is proposed within each catchment which will predominantly be dry and only fill up in larger storm events, combined with a below-ground storage area to provide the majority of the storage.

3.5.1 Surface Water Storage Estimate (Housing Development)

The hardstanding area has been calculated by assuming a runoff factor of 0.95 for the roofs and the 0.90 roads/footpaths as outlined in the CIRIA C753 SuDS Manual. Conservatively we have not deducted the storage capacity of the SuDS features in our attenuation volumes.

Table 5: Catchment 4A

	Qbar Outflow (I/s)	Duration of Critical Event	Storage Required
1:1-Year +20% Climate Change		360-minute Storm Event	251 m ³
1:30-Year +20% Climate Change	16.80 l/s	480-minute Storm Event	664 m ³
1:100-Year +20% Climate Change		480-minute Storm Event	860 m ³

It is proposed to provide sufficient attenuation capacity to cater for the 1:100-year critical storm events with 20% climate change allowed for. Refer to Appendix F for the 1, 30 & 100-year storm storage estimates.

3.6 Storm Water Calculation

The total drained area of the proposed development is approximately 45,408m² (4.54 Ha). The permitted outflow for the site is 3.7l/s/ha in accordance with the criteria set out in Section 3.4. Calculations for pipe sizes and gradients are based on stormwater runoff from the roofs and surfaced areas using the Rational Method for surface water design (Bilhams Formula), with a storm return period (N) of 5 years. Pipe capacities and velocities have been calculated using Colebrook-White formula with a roughness coefficient (Ks) of 0.6mm.

Surface water sewers will be designed and laid strictly in accordance with Fingal County Council requirements for taking in charge. It is intended that all sewers within the public domain will be handed over to Fingal County Council for taking in charge. All wayleave requirements will be assessed during the detailed design stage. All private outfall manholes will be built in accordance with the Greater Dublin Regional Code of Practice for Drainage Works. No private drainage will be located within the public areas.

Drains will be laid in accordance with the requirements of the Building Regulations, Technical Guidance Document H. Excess stormwater shall be attenuated in a detention basin consisting of above and below ground storage. The proposed storage system will gradually fill up during storm events and will release attenuated surface water after the storm at a controlled rate via a Hydro-Brake.

The calculations for the storage design are included in Appendix F of this report; these indicate that for a return period of 100 years. Refer to Appendix D for the paved area factors calculations. We conservatively have not counted the storage capacity of the permeable paving, green roofs, rain gardens and swales in our attenuation calculations. This will allow for removal of any features and future blockages / sand silting.

The following runs off rates factors have been applied to the scheme to calculate the Percentage Run-off or PIMP:

- 1. 95% from Roofs
- 2. 95% Green roofs
- 3. 90% from Roads/Hardstanding
- 4. 90% from Roads draining to SuDS features.
- 5. 95% from Permeable Paving
- 6. 5% from Grassed areas

3.6.1 Surface Water Storage Estimate

It is proposed that the attenuation for the catchment will be provided within the public open space at the centre of the site. It is proposed that this will be provided in the form of a shallow detention basin, along with storage provision below ground in a cellular attenuation system (Stormtech or similar approved, consisting of 60% voids). Refer to the summary below for the exact details:

Characteristic	Value
Cover Level	83.50 m
Above-Ground Depression Invert Level	82.90 m
Top of Water Level	83.40 m
Volume of Depression	205 m ³
Top of Stone Level	82.535 m
Stone Invert Level	80.835 m
Footprint of Underground System	703 m ²
Volume of Underground System	690 m ³
Total Volume	895 m ³

Table 6: Attenuation Provision

3.7 SUDS Selection Criteria

Sustainable Urban Drainage Systems (SUDS) have been developed and are in use to alleviate the detrimental effects of traditional urban stormwater drainage practices that typically consisted of piping runoff of rainfall from developments to the nearest receiving watercourse. Surface water drainage methods that take account of quantity, quality and amenity issues are collectively referred to as sustainable urban drainage systems; they are typically made up of one or more structures built to manage surface water runoff.

The proposed surface water drainage system for this development has been designed as a sustainable urban drainage system and uses. Roadside swales with infiltration trenches, green roofs (a minimum of 70% of the roof area of apartments will be green roof), an attenuation storage system, permeable paving together with a flow control device and petrol interceptor have been included in the design.

The proposed drainage sitewide system has been designed in such a manner that, where possible, surface water mimics the natural water cycle processes including infiltration, evaporation, transpiration, reuse and attenuation of rainfall.

A stormwater management or treatment train approach ensures that run-off quantity and quality is improved. The following objectives of the treatment train provide an integrated and balanced approach to help mitigate the changes in stormwater run-off flows that occur as land is urbanised and to help mitigate the impacts of stormwater quality on receiving systems:

- 1) Source control: conveyance and infiltration of run-off; and
- 2) Site Control: reduction in volume and rate of surface run-off, with some additional treatment provided.

The target development and design criteria for SuDS, set out in the CIRIA SuDS manual, is as follows:

- Water Quantity Ensuring that the surface water runoff from the proposed development does not have a detrimental impact on the people, property, and environment.
- Water Quality Reducing urban runoff by SuDS and increasing the quality of the water.
- Amenity Aims to deliver pleasant, attractive and good-looking urban environments.
- **Biodiversity** Creating new habitats and rehabilitating or enhancing habitats through SuDS measures.



The applicant has considered the use of all appropriate SUDS devices as part of the site SUDS strategy. All of the proposed SuDS features considered for the proposed development are highlighted below:

3.7.1 Green Roofs

These are areas of living vegetation, installed on the top of the building, for a range of reasons including visual benefit, ecological value, enhanced building performance, and the reduction of surface water run-off.



Figure 9: Typical Extensive Green Roof Schematic

It is proposed that at least 70% of the apartments' roof area be utilized for the green roof area. Conservatively we have not included any storage capacity of the green roof in our attenuation calculations.

3.7.2 Swales

Swales are shallow, flat bottomed, vegetated open channels designed to convey and treat surface water runoff. When incorporated in a site-wide design, they can enhance the natural landscape and provide aesthetic and biodiversity benefits. They will be used to drain roads where it is convenient to collect distributed inflows of runoff or as a means of conveying runoff on the surface while enhancing access corridors or other open spaces.

Swales can have a variety of profiles and can incorporate a range of different planting strategies or form part of the overall landscape development and be included as part of the play areas in some cases. It is proposed to implement shallow roadside swales at the proposed development at appropriate locations. These will typically be c. 200mm deep vegetated channels with below-ground pea gravel and a perforated pipe.





3.7.3 Detention Basin

Detention basins are landscaped depressions that are normally dry except during and immediately following storm events. They can typically be on-line/flow-through systems where surface water runoff from regular storm events is routed through the basin's below-ground stone layer and when the flows rise due to the restricted outflow, the basin fills and provides storage for the surface water runoff.

It is proposed to provide a detention basin consisting of above and below-ground storage. The belowground cellular storage system will cater for the low flow/regular storm events greater than 30 years, whereas the above-ground storage will provide attenuation in larger storm events. The attenuation system is designed so the detention basin will only fill during extreme events.

The above-ground depression will be vegetated and planted as part of the landscape architect's proposal. The detention basin, therefore, acts in a way as a bio-retention due to the positive planting/vegetation and habitual effects thereof.

3.7.4 Bioretention System / Rain Gardens / Rainwater Planters

Bioretention systems, including rain gardens, are shallow landscaped depressions that can reduce runoff. As part of the proposal for the subject site, it is proposed to utilize rain gardens and rainwater planters, rather than shallow vegetated depressions.

These are attractive landscape features that are mainly self-irrigating and self-fertilising. Boxes/planters will use rainwater runoff originating from a building/house roof and in essence, slows the flow/runoff from the roof before it enters the main drainage. A downpipe would typically discharge into these and have an overflow into the main external drainage. The most common system is a flow-through rainwater planter and will be utilized where possible.

Figure 11: Flow-Through Rainwater Planter



3.7.5 Flow Control Device

A Hydrobrake or similar approved flow control device will be used to limit the discharge to the greenfield equivalent runoff rate. It is proposed that each catchment's flow will be restricted and attenuated within its own boundaries.

3.7.6 Petrol Interceptor

A petrol interceptor is a trap to filter out pollutants and hydrocarbons from the surface water runoff. It is proposed that a petrol interceptor be installed immediately upstream of the site's overall outfall.

3.8 SUDS Maintenance

In order to comply with the County Development Plan "Development Design Standards," it is proposed to:

- Separate foul and surface water
- Include appropriate on-site disposal of surface water.
- Comply with the standards set out in the GDSDS.
- Implement appropriate SUDS measures.

All SUDS measures included will be designed in accordance with the CIRIA SUDS Manual C753 as required by the GDSDS prepared by Fingal County Council and the other Local Authorities in the Greater Dublin Area.

For the proposed SUDS strategy to work as designed, the entire drainage system must be well maintained. It will be the responsibility of the site management team to ensure the drainage system is maintained during the construction stage and initial phases of occupation. This will include maintenance and cleaning of gullies drain manholes (including catch pits) and attenuation basins will ensure adequate performance. The recommended program is outlined in the tables below.

Operation and maintenance requirements for green roofs			
Maintenance schedule	Required action	Typical frequency	
	Inspect all components including soil substrate, vegetation, drains, irrigation systems (if applicable), membranes and roof structure for proper operation, integrity of waterproofing and structural stability	Annually and after severe storms	
Regular inspections	Inspect soil substrate for evidence of erosion channels and identify any sediment sources	Annually and after severe storms	
	In spect drain inlets to ensure unrestricted runoff from the drainage layer to the conveyance or roof drain system	Annually and after severe storms	
	Inspect underside of roof for evidence of leakage	Annually and after severe storms	
Regular maintenance	Remove debris and litter to prevent clogging of inlet drains and interference with plant growth	Six monthly and annually or as required	
	During establishment (ie year one), replace dead plants as required	Monthly (but usually responsibility of manufacturer)	
	Post establishment, replace dead plants as required (where > 5% of coverage)	Annually (in autumn)	
	Remove fallen leaves and debris from deciduous plant foliage	Six monthly or as required	
	Remove nuisance and invasive vegetation, including weeds	Six monthly or as required	
	Mow grasses, prune shrubs and manage other planting (if appropriate) as required – clippings should be removed and not allowed to accumulate	Six monthly or as required	
Remedial actions	If erosion channels are evident, these should be stabilised with extra soil substrate similar to the original material, and sources of erosion damage should be identified and controlled	As required	
	If drain inlet has settled, cracked or moved, investigate and repair as appropriate	As required	

Table 7: Maintenance Schedule for Green Roofs - CIRIA C753 The SuDS Manual

Operation and maintenance requirements for swales			
Maintenance schedule	Required action	Typical frequency	
	Remove litter and debris	Monthly, or as required	
	Cut grass – to retain grass height within specified design range	Monthly (during growing season), or as required	
	Manage other vegetation and remove nuisance plants	Monthly at start, then as required	
	Inspect inlets, outlets and overflows for blockages, and clear if required	Monthly	
Regular maintenance	Inspect infiltration surfaces for ponding, compaction, silt accumulation, record areas where water is ponding for > 48 hours	Monthly, or when required	
	Inspect vegetation coverage	Monthly for 6 months, quarterly for 2 years, then half yearly	
	Inspect inlets and facility surface for silt accumulation, establish appropriate silt removal frequencies	Half yearly	
Occasional maintenance	Reseed areas of poor vegetation growth, alter plant types to better suit conditions, if required	As required or if bare soil is exposed over 10% or more of the swale treatment area	
Remedial actions	Repair erosion or other damage by re-turfing or reseeding	As required	
	Relevel uneven surfaces and reinstate design levels	As required	
	Scarify and spike topsoil layer to improve infiltration performance, break up silt deposits and prevent compaction of the soil surface	As required	
	Remove build-up of sediment on upstream gravel trench, flow spreader or at top of filter strip	As required	
	Remove and dispose of oils or petrol residues using safe standard practices	As required	

Table 8: Maintenance Schedule for Swales - CIRIA C753 The SuDS Manual

Operation and maintenance requirements for detention basins			
Maintenance schedule	Required action	Typical frequency	
	Remove litter and debris	Monthly	
	Cut grass – for spillways and access routes	Monthly (during growing season), or as required	
	Cut grass – meadow grass in and around basin	Half yearly (spring – before nesting season, and autumn)	
	Manage other vegetation and remove nuisance plants	Monthly (at start, then as required)	
	Inspect inlets, outlets and overflows for blockages, and clear if required.	Monthly	
Regular maintenance	Inspect banksides, structures, pipework etc for evidence of physical damage	Monthly	
	Inspect inlets and facility surface for silt accumulation. Establish appropriate silt removal frequencies.	Monthly (for first year), then annually or as required	
	Check any penstocks and other mechanical devices	Annually	
	Tidy all dead growth before start of growing season	Annually	
	Remove sediment from inlets, outlet and forebay	Annually (or as required)	
	Manage wetland plants in outlet pool – where provided	Annually (as set out in Chapter 23)	
	Reseed areas of poor vegetation growth	As required	
	Prune and trim any trees and remove cuttings	Every 2 years, or as required	
Occasional maintenance	Remove sediment from inlets, outlets, forebay and main basin when required	Every 5 years, or as required (likely to be minimal requirements where effective upstream source control is provided)	
	Repair erosion or other damage by reseeding or re-turfing	As required	
Remedial actions	Realignment of rip-rap	As required	
	Repair/rehabilitation of inlets, outlets and overflows	As required	
	Relevel uneven surfaces and reinstate design levels	As required	

Table 9: Maintenance Schedule for Detention Basins - CIRIA C753 The SuDS Manual

Table 10: Maintenance Schedule for Bioretention Systems - CIRIA C753 The SuDS Manual

Maintenance schedule	ce schedule Required action	
Regular inspections	Inspect infiltration surfaces for silting and ponding, record de-watering time of the facility and assess standing water levels in underdrain (if appropriate) to determine if maintenance is necessary	Quarterly
	Check operation of underdrains by inspection of flows after rain	Annually
	Assess plants for disease infection, poor growth, invasive species etc and replace as necessary	Quarterly
	Inspect inlets and outlets for blockage	Quarterly
	Remove litter and surface debris and weeds	Quarterly (or more frequently for tidiness or aesthetic reasons)
Regular maintenance	Replace any plants, to maintain planting density	As required
	Remove sediment, litter and debris build-up from around inlets or from forebays	Quarterly to biannually
Occasional maintenance	Infill any holes or scour in the filter medium, improve erosion protection if required	As required
	Repair minor accumulations of silt by raking away surface mulch, scarifying surface of medium and replacing mulch	As required
Remedial actions	Remove and replace filter medium and vegetation above	As required but likely to be > 20 years

Operation and maintenance requirements for trees (after CRWA, 2009)			
Maintenance schedule	Required action	Typical frequency	
	Remove litter and debris	Monthly (or as required)	
Regular maintenance	Manage other vegetation and remove nuisance plants	Monthly (at start, then as required)	
	Inspect inlets and outlets	Inspect monthly	
	Check tree health and manage tree appropriately	Annually	
Occasional maintenance	Remove silt build-up from inlets and surface and replace mulch as necessary	Annually, or as required	
	Water	As required (in periods of drought)	
Monitoring	Inspect silt accumulation rates and establish appropriate removal frequencies	Half yearly	

Table 11: Maintenance Schedule for Tree Pits - CIRIA C753 The SuDS Manual

Petrol and Flow Control Device Maintenance:

To perform the required maintenance for the flow control device(s) and petrol interceptor, refer to the specific manufacturers' recommendation on the frequency of maintenance and the task that should be completed.

4. Water Supply

4.1 Water Supply - General

At present, there is a water pipeline with a diameter of 300 mm that traverses the subject site, running from the southwest side of the site towards the northeast side. However, Irish Water have granted a diversion application for this watermain, under the reference DIV22229. The new route for the water pipeline diversion will start from Damastown Avenue on the north side of the site and then southwards along the new Church Fields link road. The Church Fields link road will now serve as the new route for the diverted water pipeline, servicing Church Field West to the west and the permitted Church Fields development and the proposed Church Fields East development (subject site) to the east. The subject site will be connected to the watermain network that is granted for Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21).

The impact of the water supply from the overall Church Fields development on the Irish Water network was assessed following the submission of a pre-connection enquiry form issued to Irish Water. A Confirmation of Feasibility has been issued by Irish Water on the 18th of April 2023 which confirms capacity for the subject site in the surrounding network. Please refer to Appendix A for details.

Water Mains suitable for Works and approved by Irish Water shall be either ductile iron (DI) or polyethylene (PE), with PE80 or PE100 rating (MDPE, HDPE or HPPE). The minimum depth of cover from the finished ground level to the external crown of a Water Main shall be 900mm. A greater depth of cover and/or greater strength pipe and/or a higher class of bedding may be required where high traffic loading is anticipated. Depths may be altered to avoid obstructions, including separation distances between other utility services. The desirable maximum cover for a Service Connection pipe or a Water Main should be 1200mm, where practicable.

As part of this planning application, we have submitted the wastewater & watermains design to Irish Water for design vetting. A statement of design acceptance was issued, please refer to Appendix C.

Please refer to Waterman Moylan Drawing 20-074-P300 for details of the watermain to serve the subject lands.

4.2 Water Demand Calculation

An estimate of water demand from the public water supply system for the proposed site has been based on the development of 217 units, with an average occupancy of 2.7 persons (in compliance with Irish Water – Code of Practice for Water Infrastructure). Details are shown below. The average daily demand from the public supply for the development is estimated at 87.9 m³/day.

Table 12: Calculation of approved Water Demand

	No. of	Demand	Population per Unit	Total
Description	Units /	l/h/day	/ Floor Area	Demand
				(l/d)
Apartment Units	96	150	2.7	38,880
Housing Units	121	150	2.7	49,005
				87,885 l/d

Table 13: Calculation of Proposed Water Peak Demand

Calculation of Proposed Peak Foul Flow		
Total Daily Discharge (from Table 1.)	87,885	l/d
Average Daily Consumption	1.02	l/s
Average Peak Demand (Daily Consumption x 1.25)	1.275	l/s
Peak Water Demand (=5 x Average Peak)	6.375	l/s

4.3 Water Conservation

The water demand for the development can be subdivided as follows:

• Potable / Non-potable Breakdown

Detailed studies have quantified the breakdown between potable and non-potable uses for residential uses.

The following diagram illustrates the current percentage breakdown of water usage in domestic circumstances and is from Griggs and Shouler 1994 as published in Chapter 11 of 'Water, Sanitary & Waste Services for Buildings' by Wise and Sheffield.



In addition, water conservation measures will be used, to further reduce overall water demand, including:

- Low volume flush / dual flush WC's
- Aerated shower heads
- Spray taps
- Draw off tap controls.
- Rainwater reuse water butts where applicable / raingardens
- Leak detection measures through the metering of supply
5. Roads and Transport

5.1 Site Access

Vehicular access to the site will be fed via the Church Fields Housing and Eastern Linear Park Development (Permitted under FCC Ref.: Part XI/012/21) lands to the west. The main access road to both sites will be located off Wellview Avenue roundabout traversing the overall development, currently under construction as part of the road upgrade project linking Wellview and Damastown Avenue.

5.2 Proposed Road Network

The roads have been designed to comply with Design Manual for Urban Roads and Streets (DMURS) as required by the Fingal County Development Plan 2023-2029. In this regard, the internal roads generally are generally 6.0m in width. The road network design ensures sufficient clearance for all large vehicles, including refuse and fire engine turning movements. A Stage 1 Road Safety Audit was completed by Norman Bruton Consulting Engineers as part of this planning application. The issues highlighted by the auditor have been addressed, and the site layouts are updated. Please refer to the Stage 1 Road Safety Audit submitted as part of this application.

5.3 DMURS

Waterman Moylan Consulting Engineers considers that the proposed development is consistent with the principles and guidance outlined in the Design Manual for Urban Roads and Streets (DMURS). Outlined below are some of the specific design features that have been incorporated within the proposed scheme with the objective of delivering a design that is in full compliance with DMURS.

In order of importance, DMURS prioritises pedestrians, cyclists, public transport and private cars. The proposed development has been designed with pedestrians and cyclists taking precedence over other modes of transport. In this regard, footpaths are provided throughout the development, with the required pedestrian and cyclist linkages onto the facilities in the close proximity of the site.

Active edges are recommended in DMURS to enliven the edges of the street, creating a more interesting and engaging environment. An active frontage is achieved with frequent entrances and openings that ensure the street is overlooked and generate pedestrian activity as people come and go from buildings. The roads throughout the development have regular junctions and driveways in accordance with this recommendation.

On-street parking is proposed throughout the site. On-street parking separates pedestrians from the vehicle roadway and, as per DMURS Section 4.4.9, can calm traffic by increasing driver caution, contribute to pedestrian comfort by providing a buffer between the vehicular carriageway and footpath and provide good levels of passive security. Streets have been designed in accordance with the alignment and curvature recommendations set out in DMURS Section 4.4.6.

Suitable sightlines will be provided throughout the development, ensuring that localised planting does not obscure visibility as cars make turning manoeuvres, improving pedestrian safety at crossing points.

Public areas fronting and within the proposed development will be designed by a multidisciplinary design team to accommodate pedestrians and cyclists in accordance with the appropriate principles and guidelines set out in DMURS. In particular, the vehicular access and public footways within the remit of the development will incorporate the relevant DMURS requirements and guidelines as set out above.

A full DMURS Statement is done under separate cover. Please refer to 20-074r.4006 DMURS Statement of Consistency.

5.4 **Proposed Pedestrian and Cyclist Facilities**

New footpaths will be provided in accordance with Section 4.3.1 of DMURS which suggests that a minimum 1.8m footpath should be provided on all footways. In this regard, footpaths are generally provided with a width of 2.0m. Crossing points are located at various points within the development such that unimpeded pedestrian movement is facilitated. Cyclists will be kept on-road within the proposed development. Accordingly, the proposed development is consistent with the principles outlined in DMURS.

5.5 Traffic and Transport Assessment

A full traffic and transport assessment is done under separate cover. Please refer to 20-074r.4005 Traffic and Transport Assessment.

5.6 Car Parking

The proposed development comprises a mixture of terraced housing units and apartments. It is proposed to provide long-term and visitor parking spaces for the house and apartment units. This totals c. 306 No. car parking spaces to be provided for the c. 217 No housing units.

5.7 Public Transport

The subject site is mainly served by 2 No. bus stops in the close vicinity to the site. These are Lady's Well Road Stop, c. 850m south of the subject site, and the R121 stop approximately 950m to the east.



Figure 12: Public Transport in Close Proximity to the Site

Both bus stops are located approximately 5 minute's walk from the subject site and serve the following bus routes as indicated in the below tables:

Table 14: R121 Bus Stop

Route	From	То	Weekday Services	Weekend Services	
40d Dublin Bus	Parnell St.	Tyrrelstown	46 in each direction	25 in each direction	
236/A GoAhead	IBM Campus Blanchardstown (via Tyrrelstown)		6 in each direction	N/A	
238 GoAhead	Turroletown	Mulbuddort	20 in each direction	18 in each direction (Sat.)	
	Tyneislown	Wundduart		15 in each direction (Sun.)	

Route	From	То	Weekday Services	Weekend Services
38 Dublin Bus	Damastown	Burlington Road	38 in each direction	32 in each direction
38a Dublin Bus	Damastown	Burlington Road	39 in each direction	30 in each direction
38b Dublin Bus	Damastown	Burlington Road	7 in each direction	-
220/A GoAhead	DCU	Lady's well Road	16 in each direction	16 in each direction (Sat. only)
238 GoAhead	Tyrrelstown	Mulhuddart	20 in each direction	18 in each direction (Sat.) 15 in each direction (Sun.)

Table 15: Lady's Well Road Bus Stop

5.7.1 Bus Connects

The subject site is located in close proximity to various new Bus Connects routes that will be in place in the future. The same bus stops mentioned in the section above will be served by the B3 Branch route, the L62 and L63 Local routes and the P63 Peak Time Route.

Figure 13: Bus Connects Local Area Map



The frequency of these routes are summarized in the table below:

Table 16: Bus Connects Trip Frequency

Route	From	То	Weekday Services	Weekend Services
B3-Branch	Tyrrelstown	Dun Laoghaire (via City Centre)	Generally, every 15 minutes	Generally, every 15- 30 minutes
L62	Blanchardstown	Broombridge (Via Tyrrelstown)	Generally, every 15-30 minutes	Generally, every 30- 60 minutes
L63	Damastown	Blanchardstown	Generally, every 15 minutes	Generally, every 15- 30 minutes
P63	Damastown	City Centre (Via Corduff)	From 7:00-8:00 & 15:00-17:00 every 3 minutes	N/A

5.8 Local Amenities

Further to the site being well-served by the bus network as well as the proposed future Bus Connects Network, the site is also well served by amenities in close proximity to the subject site. The table below summarises all of the amenities which is located within 15 minutes of walking from the subject site.

Table 17: Amenities within 15 minutes of walking distance.

Amenity	Distance (m)	Time
AllCare Pharmacy Mulhuddart	700	9 min
Spar Mulhuddart	850	11 min
Hillview Stores	650	8 min
Maxwell Hair & Beauty	650	8 min
Hopkins Park	700	8 min
Jorag Stores	700	9 min
Gaelscoil an Chuilinn	1000	13 min

Most of these amenities will be accessed via a quicker route once the linear park to the south of the subject site is completed.

5.9 Conclusion

The subject development is fully Design Manual for Urban Roads and Streets (DMURS) compliant and all roads, local streets, on-street parking and pedestrian/cycling facilities has been designed to keep the hierarchy of road users in mind as specified in the DMURS Manual. The site is well served with public transport with various transport options available to commute into the city center with the future Bus Connects transport extension project only further enhancing this. The site is generally located close to amenities, however, if need be to travel any further, any of the transport options can easily be accessed/utilized.

Appendix A

Irish Water Confirmation of Feasibility – Church Fields lands (1,000 units)

CONFIRMATION OF FEASIBILITY



Noel Mahon

Waterman Moylan Block S Eastpoint Business Park, Alfie Byrne Road D03H3F4

18 April 2023

Our Ref: CDS23001981 Pre-Connection Enquiry Sectors 1, 2, 3, 4, Church Fields, Tyrrelstown, Dublin

Dear Applicant/Agent,

We have completed the review of the Pre-Connection Enquiry.

Irish Water has reviewed the pre-connection enquiry in relation to a Water & Wastewater connection for a Housing Development of 1,000 unit(s) at Sectors 1, 2, 3, 4, Church Fields, Tyrrelstown, Dublin, (the **Development)**.

Based upon the details provided we can advise the following regarding connecting to the networks;

- Water Connection
 Feasible without infrastructure upgrade by
 Irish Water
- Primary connection main should be a 300mm ID pipe connected to the existing 300mm DI main, as proposed by the Applicant.
- Secondary connection main should be a 300mm ID pipe connected to the existing 300mm DI main at Damastown Avenue Roundabout with installation of a control valve on the line. The valve should be closed during normal operation and opened at times of emergency.



Stiúrthóirí / Directors: Tony Keohane (Chairman), Niall Gleeson (CEO), Christopher Banks, Fred Barry, Gerard Britchfield, Liz Joyce, Patricia King, Eileen Maher, Cathy Mannion, Michael Walsh

Oifig Chláraithe / Registered Office: Teach Colvill, 24–26 Sráid Thalbóid, Baile Átha Cliath 1, D01 NP86 / Colvill House, 24–26 Talbot Street, Dublin 1 D01 NP86 Is cuideachta ghníomhaíochta ainmnithe atá faoi theorainn scaireanna é Uisce Éireann / Irish Water is a designated activity company, limited by shares. Uimhir Chláraithe in Éirinn / Registered in Ireland No.: 530363 **Uisce Éireann** Bosca OP 448 Oifig Sheachadta na Cathrach Theas Cathair Chorcaí

Irish Water PO Box 448, South City Delivery Office, Cork City.

www.water.ie

- The proposed Development indicates that Irish Water assets are present on the site. The Developer has to demonstrate that proposed structures and works will not inhibit access for maintenance or endanger structural or functional integrity of the assets during and after the works. Drawings (showing clearance distances, changing to ground levels) and Method Statements should be included in the Detailed Design of the Development. A wayleave in favour of Irish Water will be required over the assets that are not located within the Public Space. For design submissions and queries related to diversion/build near or over, please contact IW Diversion Team via email address <u>diversions@water.ie</u>

Wastewater Connection

Feasible without infrastructure upgrade by Irish Water

- The Development should be connected to the existing 750 CO gravity sever as proposed by the Applicant (via proposed foul sewer within the site boundaries, granted under CDS2200712901 connection application).
- The proposed Development indicates that Irish Water assets are present on the site. The Developer has to demonstrate that proposed structures and works will not inhibit access for maintenance or endanger structural or functional integrity of the assets during and after the works. Drawings (showing clearance distances, changing to ground levels) and Method Statements should be included in the Detailed Design of the Development. A wayleave in favour of Irish Water will be required over the assets that are not located within the Public Space. For design submissions and queries related to diversion/build near or over, please contact IW Diversion Team via email address <u>diversions@water.ie</u>

This letter does not constitute an offer, in whole or in part, to provide a connection to any Irish Water infrastructure. Before the Development can be connected to our network(s) you must submit a connection application and be granted and sign a connection agreement with Irish Water.

As the network capacity changes constantly, this review is only valid at the time of its completion. As soon as planning permission has been granted for the Development, a completed connection application should be submitted. The connection application is available at <u>www.water.ie/connections/get-connected/</u>

Where can you find more information?

- Section A What is important to know?
- Section B Details of Irish Water's Network(s)

This letter is issued to provide information about the current feasibility of the proposed connection(s) to Irish Water's network(s). This is not a

connection offer and capacity in Irish Water's network(s) may only be secured by entering into a connection agreement with Irish Water.

For any further information, visit <u>www.water.ie/connections</u>, email <u>newconnections@water.ie</u> or contact 1800 278 278.

Yours sincerely,

Nonne Maesis

Yvonne Harris Head of Customer Operations

Section A - What is important to know?

What is important to know?	Why is this important?
Do you need a contract to connect?	• Yes, a contract is required to connect. This letter does not constitute a contract or an offer in whole or in part to provide a connection to Irish Water's network(s).
	 Before the Development can connect to Irish Water's network(s), you must submit a connection application <u>and</u> <u>be granted and sign</u> a connection agreement with Irish Water.
When should I submit a Connection Application?	A connection application should only be submitted after planning permission has been granted.
Where can I find information on connection charges?	Irish Water connection charges can be found at: <u>https://www.water.ie/connections/information/charges/</u>
Who will carry out the connection work?	 All works to Irish Water's network(s), including works in the public space, must be carried out by Irish Water*.
	*Where a Developer has been granted specific permission and has been issued a connection offer for Self-Lay in the Public Road/Area, they may complete the relevant connection works
Fire flow Requirements	• The Confirmation of Feasibility does not extend to fire flow requirements for the Development. Fire flow requirements are a matter for the Developer to determine.
	What to do? - Contact the relevant Local Fire Authority
Plan for disposal of storm water	The Confirmation of Feasibility does not extend to the management or disposal of storm water or ground waters.
	• What to do? - Contact the relevant Local Authority to discuss the management or disposal of proposed storm water or ground water discharges.
Where do I find details of Irish Water's network(s)?	 Requests for maps showing Irish Water's network(s) can be submitted to: <u>datarequests@water.ie</u>

What are the design requirements for the connection(s)?	 The design and construction of the Water & Wastewater pipes and related infrastructure to be installed in this Development shall comply with <i>the Irish Water</i> <i>Connections and Developer Services Standard Details</i> <i>and Codes of Practice,</i> available at <u>www.water.ie/connections</u>
Trade Effluent Licensing	 Any person discharging trade effluent** to a sewer, must have a Trade Effluent Licence issued pursuant to section 16 of the Local Government (Water Pollution) Act, 1977 (as amended).
	 More information and an application form for a Trade Effluent License can be found at the following link: <u>https://www.water.ie/business/trade-effluent/about/</u> **trade effluent is defined in the Local Government (Water Pollution) Act, 1977 (as amended)
	**trade effluent is defined in the Local Government (Water Pollution) Act, 1977 (as amended)

Section B – Details of Irish Water's Network(s)

The map included below outlines the current Irish Water infrastructure adjacent the Development: To access Irish Water Maps email datarequests@water.ie



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Note: The information provided on the included maps as to the position of Irish Water's underground network(s) is provided as a general guide only. The information is based on the best available information provided by each Local Authority in Ireland to Irish Water.

Whilst every care has been taken in respect of the information on Irish Water's network(s), Irish Water assumes no responsibility for and gives no guarantees, undertakings or warranties concerning the accuracy, completeness or up to date nature of the information provided, nor does it accept any liability whatsoever arising from or out of any errors or omissions. This information should not be solely relied upon in the event of excavations or any other works being carried out in the vicinity of Irish Water's underground network(s). The onus is on the parties carrying out excavations or any other works to ensure the exact location of Irish Water's underground network(s) is identified prior to excavations or any other works being carried out. Service connection pipes are not generally shown but their presence should be anticipated.

Appendix B Wastewater Pipe Design

> 38 Engineering Assessment Report Project Number: 20-074 Document Reference: 20-074r.4001



Page 1 20-074 Church Fields Church Field East Foul Network

Design Settings

Frequency of use (kDU)	1.00	Minimum Velocity (m/s)	1.00
Flow per dwelling per day (I/day)	405	Connection Type	Level Soffits
Domestic Flow (I/s/ha)	0.0	Minimum Backdrop Height (m)	0.600
Industrial Flow (I/s/ha)	0.0	Preferred Cover Depth (m)	1.200
Additional Flow (%)	10	Include Intermediate Ground	\checkmark

<u>Nodes</u>

Name	Dwellings	Cover	Manhole	Easting	Northing	Depth
		Level	Туре	(m)	(m)	(m)
F 4	-	(m)		707005 006	744570.050	4 405
F1	3	83.600	Adoptable	707005.326	741579.052	1.495
F2	17	82.8/1	Adoptable	706963.959	741575.011	1.286
F3	6	84.895	Adoptable	707028.423	741537.180	1.942
F4	20	85.950	Adoptable	707064.462	741541.033	1.425
F5	12	85.125	Adoptable	707031.436	741505.506	2.331
	6	84.895	Adoptable	707034.544	741471.713	2.271
	3	83.970	Adoptable	706998.195	741468.889	1.528
	3	84.393 94 1 47	Adoptable	707038.764	741423.000	2.000
F9 F10	2	84.147	Adoptable	707021.891	741422.038	2.324
	Z	83.405 93.105	Adoptable	706985.830	741432.182	1.708
F11 F12	4	03.105	Adoptable	706978.290	741428.878	1.569
F12	4	83.323	Adoptable	706977.003	741412.259	1.812
F13	3	83.000	Adoptable	706964.126	741370.748	1.707
F14 F1F	4	82.760	Adoptable	706957.466	741344.112	1.604
F15 F16	2 10	82.900	Adoptable	700971.338	741340.945	1.518
F10 F17	19	83.750	Adoptable	707005.537	741332.070	1.425
F1/ E10	10	02.990 02.20E	Adoptable	700907.570	741320.119	1.425
F10 E10	1	03.393	Adoptable	700901.784	741304.555	2 /02
F19 F20	4	04.400 04.200	Adoptable	707035.477	741413.400	2.495
F20 E21	0	04.200 95 047	Adoptable	707023.000	741302.781	1.550
FZ1 F22	4	86 / 20	Adoptable	707092.882	741428.839	1 000
FZZ E22	4	00.450 96 760	Adoptable	707099.214	741434.390	2.095
F23 F24	22	86 500	Adoptable	707095.102	741401.430	2.005
	52	83 330	Adoptable	707089.071	741341.443	1.425
F26		82 395		706950 213	741405.997	1.177
F27		82 161	Adoptable	706939 512	741309 864	1 4 2 5
F28	А	81 245	Adoptable	706903 694	741305.004	1 4 2 5
F29	-	80 770	Adoptable	706888 134	741330 429	1.425
FHM 48		79 870	Adoptable	706889 314	741338 230	1 512
F30	6	83 135	Adoptable	706968 668	741379 561	1 792
F31	Ũ	80 989	Adoptable	706891 183	741373 413	1 586
FMH - 1		82 690	Adoptable	706964 840	741560 310	1 350
FMH3A		84 625	Adoptable	707027 303	741548 888	1 400
FW-2.1		84.789	Adoptable	707036.030	741454.775	1.350



		Water	man Mo	ylan Cons	sulting	File:	4A with	foul R.02.	pfd	Page 2				
						Netv	work: for	ll.		20-074 Church Fields				
						Sidh	arth Kur	ella		Church Field East				
						2023	3-03-20			Foul N	etwork			
	Links													
Name	e U	S	DS	Length	ks (mn	n) /	US IL	DS IL	Fall	Slope	Dia			
	No	de	Node	(m)	n		(m)	(m)	(m)	(1:X)	(mm)			
8.000_	1 F1	F	2	41.564	1.5	500	82.105	81.585	0.520	79.9	150			
7.001	F2	F	MH - 1	14.728	1.5	500	81.585	81.340	0.245	60.1	150			
3.000	F4	F	3	36.244	1.5	500	84.525	84.072	0.453	80.0	225			
5.001_	1 F3	F	5	31.817	1.5	500	82.953	82.794	0.159	200.0	225			
5.002_	1 F5	F	6	33.936	1.5	500	82.794	82.624	0.170	200.0	225			
8.000	F7	F	MH 4	27.860	1.5	500	82.442	82.153	0.289	96.4	225			
5.003	F6	F	7	36.459	1.5	500	82.624	82.442	0.182	200.0	225			
7.000_	_1 FW	-2.1 F	6	17.003	1.5	500	83.439	82.699	0.740	23.0	150			
1.001	F24	F	23	60.264	1.5	500	85.075	84.675	0.400	150.7	225			
1.002	F23	F	22	47.015	1.5	500	84.675	84.440	0.235	200.1	225			
1.003	F22	F	21	8.540	1.5	500	84.440	84.383	0.057	149.8	225			
1.004	F21	F	8	54.373	1.5	500	84.383	83.147	1.236	44.0	225			
1.014_	1 F28	F	31	13.355	1.5	500	79.820	79.403	0.417	32.0	225			
5.000	F20	F	19	38.308	1.5	500	82.850	81.975	0.875	43.8	225			
4.001	F19	F	8	10.166	1.5	500	81.975	81.907	0.068	149.5	225			
1.004_	1 F8	F	9	16.900	1.5	500	81.907	81.823	0.084	201.2	225			
1.005	F9	F	10	37.297	1.5	500	81.823	81.637	0.186	200.5	225			
1.006	F10	F	11	8.232	1.5	500	81.637	81.596	0.041	200.8	225			
1.007	F11	F	12	16.631	1.5	500	81.596	81.513	0.083	200.4	225			
1.008	F12	F	30	33.913	1.5	500	81.513	81.343	0.170	199.5	225			
1.009	F30	F	13	9.915	1.5	500	81.343	81.293	0.050	198.3	225			
1.010	F13	F	14	27.456	1.5	500	81.293	81.156	0.137	200.4	225			
7.000	F16	F	15	35.332	1.5	500	82.325	81.442	0.883	40.0	225			
5.002	F15	F	14	14.229	1.5	500	81.442	81.156	0.286	49.8	225			
Pro Vel	Vel	Сар	Flow	US	DS	ΣAr	ea ΣC	wellings	Σ Units	Σ Add	Pro	Pro		
@ 1/3 Q	(m/s)	(I/s)	(I/s)	Depth	Depth	(ha	a)	(ha)	(ha)	Inflow	/ Depth	Velocity		
(m/s)				(m)	(m)					(ha)	(mm)	(m/s)		
0.097	0.980	17.3	0.0	1.345	1.136	0.0	00	3	0.0	0.0) 4	0.133		
0.192	1.131	20.0	0.1	1.136	1.200	0.0	00	20	0.0	0.0) 8	0.274		
0.162	1.284	51.0	0.1	1.200	0.598	0.0	00	20	0.0	0.0) 7	0.228		
0 1 2 0	0 810	22.2	01	1 717	2 106	0.0	00	26	0.0	0.0) 11	0 101		

Name	Pro Vel	Vel	Сар	Flow	US	DS	Σ Area	Σ Dwellings	Σ Units	Σ Add	Pro	Pro
	@ 1/3 Q	(m/s)	(I/s)	(I/s)	Depth	Depth	(ha)	(ha)	(ha)	Inflow	Depth	Velocity
	(m/s)				(m)	(m)				(ha)	(mm)	(m/s)
8.000_1	0.097	0.980	17.3	0.0	1.345	1.136	0.000	3	0.0	0.0	4	0.133
7.001	0.192	1.131	20.0	0.1	1.136	1.200	0.000	20	0.0	0.0	8	0.274
3.000	0.162	1.284	51.0	0.1	1.200	0.598	0.000	20	0.0	0.0	7	0.228
5.001_1	0.129	0.810	32.2	0.1	1.717	2.106	0.000	26	0.0	0.0	11	0.191
5.002_1	0.143	0.810	32.2	0.2	2.106	2.046	0.000	38	0.0	0.0	13	0.213
8.000	0.208	1.169	46.5	0.2	1.303	0.952	0.000	47	0.0	0.0	12	0.293
5.003	0.155	0.810	32.2	0.2	2.046	1.303	0.000	44	0.0	0.0	14	0.223
7.000_1	0.000	1.833	32.4	0.0	1.200	2.046	0.000	0	0.0	0.0	0	0.000
1.001	0.150	0.934	37.1	0.2	1.200	1.860	0.000	32	0.0	0.0	11	0.221
1.002	0.155	0.810	32.2	0.2	1.860	1.765	0.000	40	0.0	0.0	14	0.223
1.003	0.166	0.937	37.2	0.2	1.765	1.339	0.000	44	0.0	0.0	13	0.246
1.004	0.252	1.733	68.9	0.2	1.339	1.223	0.000	44	0.0	0.0	10	0.388
1.014_1	0.396	2.032	80.8	0.6	1.200	1.361	0.000	119	0.0	0.0	15	0.591
5.000	0.113	1.737	69.1	0.0	1.125	2.268	0.000	6	0.0	0.0	4	0.188
4.001	0.100	0.938	37.3	0.1	2.268	2.463	0.000	10	0.0	0.0	7	0.151
1.004_1	0.167	0.808	32.1	0.3	2.463	2.099	0.000	57	0.0	0.0	15	0.243
1.005	0.167	0.809	32.2	0.3	2.099	1.543	0.000	59	0.0	0.0	15	0.243
1.006	0.179	0.808	32.1	0.3	1.543	1.364	0.000	61	0.0	0.0	16	0.253
1.007	0.179	0.809	32.2	0.3	1.364	1.587	0.000	61	0.0	0.0	16	0.253
1.008	0.180	0.811	32.2	0.3	1.587	1.567	0.000	65	0.0	0.0	16	0.253
1.009	0.180	0.813	32.3	0.4	1.567	1.542	0.000	71	0.0	0.0	17	0.264
1.010	0.191	0.809	32.2	0.4	1.542	1.379	0.000	74	0.0	0.0	17	0.262
7.000	0.197	1.817	72.3	0.1	1.200	1.293	0.000	19	0.0	0.0	7	0.295
5.002	0.237	1.629	64.8	0.2	1.293	1.379	0.000	37	0.0	0.0	9	0.341

			Water	man Mo	ylan Cons	ulting	File:	4A with	foul R.02.	pfd	Page 3			
CALIC							Network: foul				20-074	Church Fie	elds	
CAUS	EVVAI						Sidharth Kurella				Church Field East			
							2023-03-20				Foul Network			
						<u>Lin</u>	<u>ks</u>							
	Name	e L	JS	DS	Length	ks (mm	1) /	US IL	DS IL	Fall	Slope	Dia		
		No	ode	Node	(m)	n		(m)	(m)	(m)	(1:X)	(mm)		
	5.001	F17	'F	15	15.296	1.5	500	81.565	81.442	0.123	124.4	225		
	1.012	F14	↓ F	26	29.200	1.5	500	81.156	80.963	0.193	151.3	225		
	6.000	F18	B F	17	22.328	1.5	500	81.970	81.565	0.405	55.1	225		
	1.013	F26	5 F	27	9.482	1.5	500	80.963	80.736	0.227	41.8	225		
	1.014	F27	' F	28	22.894	1.5	500	80.736	79.820	0.916	25.0	225		
	1.015	F31	. F	29	7.650	1.5	500	79.403	79.164	0.239	32.0	225		
	1.016	F29) F	HM 48	13.259	1.5	500	79.164	78.358	0.806	16.5	225		
	3.000_	1 FM	H3A F	3	11.762	1.5	500	83.225	83.028	0.197	59.7	150		
Name	Pro Vel	Vel	Сар	Flow	US	DS	ΣΑι	rea Σl	Dwellings	Σ Units	Σ Add	Pro	Pro	
	@ 1/3 Q	(m/s)	(I/s)	(I/s)	Depth	Depth	(h	a)	(ha)	(ha)	Inflow	Depth	Velocity	
	(m/s)				(m)	(m)					(ha)	(mm)	(m/s)	
5.001	0.129	1.029	40.9	0.1	1.200	1.293	0.0	000	16	0.0	0.0	7	0.182	
1.012	0.233	0.932	37.1	0.6	1.379	1.207	0.0	000	115	0.0	0.0	20	0.334	
6.000	0.000	1.548	61.5	0.0	1.200	1.200	0.0	000	0	0.0	0.0	0	0.000	
1.013	0.373	1.779	70.7	0.6	1.207	1.200	0.0	000	115	0.0	0.0	15	0.517	
1.014	0.449	2.301	91.5	0.6	1.200	1.200	0.0	000	115	0.0	0.0	14	0.640	
1.015	0.396	2.033	80.8	0.6	1.361	1.381	0.0	000	119	0.0	0.0	15	0.591	
1.016	0.510	2.837	112.8	0.6	1.381	1.287	0.0	000	119	0.0	0.0	12	0.716	
3.000_1	0.000	1.135	20.1	0.0	1.250	1.717	0.0	000	0	0.0	0.0	0	0.000	

Pipeline Schedule

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
8.000_1	41.564	79.9	150	Circular	83.600	82.105	1.345	82.871	81.585	1.136
7.001	14.728	60.1	150	Circular	82.871	81.585	1.136	82.690	81.340	1.200
3.000	36.244	80.0	225	Circular	85.950	84.525	1.200	84.895	84.072	0.598
5.001_1	31.817	200.0	225	Circular	84.895	82.953	1.717	85.125	82.794	2.106
5.002_1	33.936	200.0	225	Circular	85.125	82.794	2.106	84.895	82.624	2.046
8.000	27.860	96.4	225	Circular	83.970	82.442	1.303	83.330	82.153	0.952
5.003	36.459	200.0	225	Circular	84.895	82.624	2.046	83.970	82.442	1.303
7.000_1	17.003	23.0	150	Circular	84.789	83.439	1.200	84.895	82.699	2.046
1.001	60.264	150.7	225	Circular	86.500	85.075	1.200	86.760	84.675	1.860
1.002	47.015	200.1	225	Circular	86.760	84.675	1.860	86.430	84.440	1.765
1.003	8.540	149.8	225	Circular	86.430	84.440	1.765	85.947	84.383	1.339
1.004	54.373	44.0	225	Circular	85.947	84.383	1.339	84.595	83.147	1.223

Link	US	Dia	Node	MH	DS	Dia	Node	MH
	Node	(mm)	Туре	Туре	Node	(mm)	Туре	Туре
8.000_1	F1	1200	Manhole	Adoptable	F2	1200	Manhole	Adoptable
7.001	F2	1200	Manhole	Adoptable	FMH - 1	1200	Manhole	Adoptable
3.000	F4	1200	Manhole	Adoptable	F3	1200	Manhole	Adoptable
5.001_1	F3	1200	Manhole	Adoptable	F5	1200	Manhole	Adoptable
5.002_1	F5	1200	Manhole	Adoptable	F6	1200	Manhole	Adoptable
8.000	F7	1200	Manhole	Adoptable	FMH 4	1200	Manhole	Adoptable
5.003	F6	1200	Manhole	Adoptable	F7	1200	Manhole	Adoptable
7.000_1	FW-2.1	1200	Manhole	Adoptable	F6	1200	Manhole	Adoptable
1.001	F24	1200	Manhole	Adoptable	F23	1200	Manhole	Adoptable
1.002	F23	1200	Manhole	Adoptable	F22	1200	Manhole	Adoptable
1.003	F22	1200	Manhole	Adoptable	F21	1200	Manhole	Adoptable
1.004	F21	1200	Manhole	Adoptable	F8	1200	Manhole	Adoptable

CAUSEW	AY 🛟	Wate	rman Mo	oylan Cons	ulting Pipeline S	File: 4A w Network: Sidharth k 2023-03-2 Schedule	ith foul R.02 foul Kurella 20	.pfd	Page 4 20-074 (Church I Foul Net	Church Fields Field East twork
Link	Length	Slope	Dia	Link	US CL	US IL	US Depth	DS CL	DS IL	DS Depth
	(m)	(1:X)	(mm)	Туре	(m)	(m)	(m)	(m)	(m)	(m)
1.014_1	13.355	32.0	225	Circular	81.245	79.820	1.200	80.989	79.403	1.361
5.000	38.308	43.8	225	Circular	84.200	82.850	1.125	84.468	81.975	2.268
4.001	10.166	149.5	225	Circular	84.468	81.975	2.268	84.595	81.907	2.463
1.004_1	16.900	201.2	225	Circular	84.595	81.907	2.463	84.147	81.823	2.099
1.005	37.297	200.5	225	Circular	84.147	81.823	2.099	83.405	81.637	1.543
1.006	8.232	200.8	225	Circular	83.405	81.637	1.543	83.185	81.596	1.364
1.007	16.631	200.4	225	Circular	83.185	81.596	1.364	83.325	81.513	1.587
1.008	33.913	199.5	225	Circular	83.325	81.513	1.587	83.135	81.343	1.567
1.009	9.915	198.3	225	Circular	83.135	81.343	1.567	83.060	81.293	1.542
1.010	27.456	200.4	225	Circular	83.060	81.293	1.542	82.760	81.156	1.379
7.000	35.332	40.0	225	Circular	83.750	82.325	1.200	82.960	81.442	1.293
5.002	14.229	49.8	225	Circular	82.960	81.442	1.293	82.760	81.156	1.379
5.001	15.296	124.4	225	Circular	82.990	81.565	1.200	82.960	81.442	1.293
1.012	29.200	151.3	225	Circular	82.760	81.156	1.379	82.395	80.963	1.207
6.000	22.328	55.1	225	Circular	83.395	81.970	1.200	82.990	81.565	1.200
1.013	9.482	41.8	225	Circular	82.395	80.963	1.207	82.161	80.736	1.200
1.014	22.894	25.0	225	Circular	82.161	80.736	1.200	81.245	79.820	1.200
1.015	7.650	32.0	225	Circular	80.989	79.403	1.361	80.770	79.164	1.381
1.016	13.259	16.5	225	Circular	80.770	79.164	1.381	79.870	78.358	1.287
3.000_1	11.762	59.7	150	Circular	84.625	83.225	1.250	84.895	83.028	1.717

Link	US	Dia	Node	MH	DS	Dia	Node	MH
	Node	(mm)	Туре	Туре	Node	(mm)	Туре	Туре
1.014_1	F28	1200	Manhole	Adoptable	F31	1200	Manhole	Adoptable
5.000	F20	1200	Manhole	Adoptable	F19	1200	Manhole	Adoptable
4.001	F19	1200	Manhole	Adoptable	F8	1200	Manhole	Adoptable
1.004_1	F8	1200	Manhole	Adoptable	F9	1200	Manhole	Adoptable
1.005	F9	1200	Manhole	Adoptable	F10	1200	Manhole	Adoptable
1.006	F10	1200	Manhole	Adoptable	F11	1200	Manhole	Adoptable
1.007	F11	1200	Manhole	Adoptable	F12	1200	Manhole	Adoptable
1.008	F12	1200	Manhole	Adoptable	F30	1200	Manhole	Adoptable
1.009	F30	1200	Manhole	Adoptable	F13	1200	Manhole	Adoptable
1.010	F13	1200	Manhole	Adoptable	F14	1200	Manhole	Adoptable
7.000	F16	1200	Manhole	Adoptable	F15	1200	Manhole	Adoptable
5.002	F15	1200	Manhole	Adoptable	F14	1200	Manhole	Adoptable
5.001	F17	1200	Manhole	Adoptable	F15	1200	Manhole	Adoptable
1.012	F14	1200	Manhole	Adoptable	F26	1200	Manhole	Adoptable
6.000	F18	1200	Manhole	Adoptable	F17	1200	Manhole	Adoptable
1.013	F26	1200	Manhole	Adoptable	F27	1200	Manhole	Adoptable
1.014	F27	1200	Manhole	Adoptable	F28	1200	Manhole	Adoptable
1.015	F31	1200	Manhole	Adoptable	F29	1200	Manhole	Adoptable
1.016	F29	1200	Manhole	Adoptable	FHM 48	1200	Manhole	Adoptable
3.000_1	FMH3A	1200	Manhole	Adoptable	F3	1200	Manhole	Adoptable



Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)
F1	707005.326	741579.052	83.600	1.495	1200				
						₀←			
						0	8.000 1	82.105	150
F2	706963.959	741575.011	82.871	1.286	1200	1	8.000_1	81.585	150
							7 001	81 585	150
F3	707028.423	741537.180	84.895	1.942	1200	1, 1	3.000 1	83.028	150
						2 2	3.000	84.072	225
						\downarrow	F 001 1	02.052	225
F4	707064.462	741541.033	85.950	1.425	1200	0 U	5.001_1	82.953	225
17	707004.402	/ 10 11.000	05.550	1.425	1200	\bigcirc			
						oet			
	707021 426		05 125	2 2 2 1	1200	0	3.000	84.525	225
гэ	/0/031.430	/41505.500	85.125	2.331	1200		5.001_1	82.794	225
						φ			
						<mark>0 0</mark>	5.002_1	82.794	225
F6	707034.544	741471.713	84.895	2.271	1200		7.000_1	82.699	150
						0 ←	5.002_1	82.624	225
						1 0	5.003	82.624	225
F7	706998.195	741468.889	83.970	1.528	1200	1	5.003	82.442	225
						0 ← _ 1			
						0	8.000	82.442	225
F8	707038.764	741423.600	84.595	2.688	1200	1	4.001	81.907	225
						0 ← 1 2 2	1.004	83.147	225
							1 00/ 1	81 007	225
F9	707021.891	741422.638	84.147	2.324	1200	1 0	1.004_1	81.823	225
						0 < - 1			
							1.005	04 022	225
F10	706985 836	741432 182	83 405	1 768	1200	0	1.005	81.823	225
110	/00505.050	741452.162	05.405	1.700	1200		1.005	01.007	225
						0 - 1			
F11	700070 200	741420.070	02 105	1 5 0 0	1200	0	1.006	81.637	225
FII	/069/8.296	/41428.8/8	83.185	1.589	1200		1.006	81.596	225
						φ			
						0 0	1.007	81.596	225
F12	706977.663	741412.259	83.325	1.812	1200		1.007	81.513	225
						\bigcirc			
						<u>م</u> لا 0	1.008	81.513	225
F13	706964.126	741370.748	83.060	1.767	1200	1 1	1.009	81.293	225
						\square			
						, т • п	1.010	81.293	225
							1	01.200	



Page 6 20-074 Church Fields Church Field East Foul Network

Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	;	Link	IL (m)	Dia (mm)
F14	706957.466	741344.112	82.760	1.604	1200	2	1	5.002	81.156	225
						(-)	2	1.010	81.156	225
						o	0	1.012	81.156	225
F15	706971.338	741340.945	82.960	1.518	1200		1	7.000	81.442	225
						0 ←	2	5.001	81.442	225
						2	0	5.002	81.442	225
F16	707005.537	741332.070	83.750	1.425	1200	0 <				
F4 7	700007 570	744226 440	02.000	4 425	4200		0	7.000	82.325	225
F1/	/06967.576	/41326.119	82.990	1.425	1200	ϕ	1	6.000	81.565	225
						1′	0	5.001	81.565	225
F18	706961.784	741304.555	83.395	1.425	1200					
							0	6.000	81.970	225
F19	707039.477	741413.460	84.468	2.493	1200		1	5.000	81.975	225
						/ 1	0	4.001	81.975	225
F20	707025.606	741362.781	84.200	1.350	1200	Č				
							0	5.000	82.850	225
F21	707092.882	741428.859	85.947	1.564	1200	0 <	1	1.003	84.383	225
522	707000 244	744424 500	06 420	1 000	1200		0	1.004	84.383	225
F22	707099.214	741434.590	86.430	1.990	1200		1	1.002	84.440	225
522	707005 4 62	744404 400	06 760	2.005	4200		0	1.003	84.440	225
F23	707095.162	741481.430	86.760	2.085	1200		1	1.001	84.675	225
						Ő	0	1.002	84.675	225
F24	707089.671	741541.443	86.500	1.425	1200	Q				
						0	0	1.001	85.075	225
FMH 4	706970.486	741465.997	83.330	1.177	1200	-1	1	8.000	82.153	225
F26	706950.213	741315.828	82.395	1.432	1200	J	1	1.012	80.963	225
						0 -	0	1.013	80.963	225



Page 7 20-074 Church Fields Church Field East Foul Network

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connection	S	Link	IL (m)	Dia (mm)
F27	706939.512	741309.864	82.161	1.425	1200	0 < _ 1	1	1.013	80.736	225
							0	1.014	80.736	225
F28	706903.694	741318.742	81.245	1.425	1200	0 ~1	1	1.014	79.820	225
							0	1.014_1	79.820	225
F29	706888.134	741330.429	80.770	1.606	1200		1	1.015	79.164	225
						1	0	1.016	79.164	225
FHM 48	706889.314	741338.230	79.870	1.512	1200		1	1.016	78.358	225
						\bigcap_{1}				
F30	706968.668	741379.561	83.135	1.792	1200	Å	1	1.008	81.343	225
						oK	0	1.009	81.343	225
F31	706891.183	741323.413	80.989	1.586	1200	0	1	1.014_1	79.403	225
							0	1.015	79.403	225
FMH - 1	706964.840	741560.310	82.690	1.350	1200		1	7.001	81.340	150
FMH3A	707027.303	741548.888	84.625	1.400	1200	P				
	707026 020	744454 775	04 700	1 252	1200	ŏ	0	3.000_1	83.225	150
FW-2.1	707036.030	/41454.//5	84.789	1.350	1200	e d				
							0	7.000_1	83.439	150

Appendix C Statement of Design Acceptance – IW

> 39 Engineering Assessment Report Project Number: 20-074 Document Reference: 20-074r.4001



Noel Mahon Waterman Moylan Block S Eastpoint Business Park Alfie Byrne Road Dublin D03H3F4

Irish Water PO Box 448, South City Delivery Office, Cork City.

Uisce Éireann Bosca OP 448

Cathrach Theas

Cathair Chorcal

Oifig Sheachadta na

www.water.ie

Re: Design Submission for Church Fields East, Tyrrelstown, Dublin (the "Development") (the "Design Submission") / Connection Reference No: CDS23001981

Dear Noel Mahon,

18 May 2023

Many thanks for your recent Design Submission.

We have reviewed your proposal for the connection(s) at the Development. Based on the information provided, which included the documents outlined in Appendix A to this letter, Irish Water has no objection to your proposals.

This letter does not constitute an offer, in whole or in part, to provide a connection to any Irish Water infrastructure. Before you can connect to our network you must sign a connection agreement with Irish Water. This can be applied for by completing the connection application form at <u>www.water.ie/connections</u>. Irish Water's current charges for water and wastewater connections are set out in the Water Charges Plan as approved by the Commission for Regulation of Utilities (CRU)(<u>https://www.cru.ie/document_group/irish-waters-water-charges-plan-2018/</u>).

You the Customer (including any designers/contractors or other related parties appointed by you) is entirely responsible for the design and construction of all water and/or wastewater infrastructure within the Development which is necessary to facilitate connection(s) from the boundary of the Development to Irish Water's network(s) (the "**Self-Lay Works**"), as reflected in your Design Submission. Acceptance of the Design Submission by Irish Water does not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works.

If you have any further questions, please contact your Irish Water representative: Name: Antonio Garzón Phone: 087 475 0587 Email: antonio.garzonmielgo@water.ie

Yours sincerely,

Monne Massis

Yvonne Harris Head of Customer Operations

Stiúrthóirí / Directors: Tony Keohane (Chairman), Niall Gleeson (CEO), Christopher Banks, Fred Barry, Gerard Britchfield, Liz Joyce, Patricia King, Eileen Maher, Cathy Mannion, Michael Walsh

Oifig Chláraithe / Registered Office: Teach Colvill, 24–26 Sráid Thalbóid, Baile Átha Cliath 1, D01 NP86 / Colvill House, 24–26 Talbot Street, Dublin 1 D01 NP86 Is cuideachta ghníomhaíochta ainmnithe atá faoi theorainn scaireanna é Uisce Éireann / Irish Water is a designated activity company, limited by shares. Uimhir Chláraithe in Éirinn / Registered in Ireland No.: 530363

Appendix A

Document Title & Revision

- 20-074 P4200 Proposed Drainage Layout Sector 4 Sheet 1 of 2
- 20-074 P4201 Proposed Drainage Layout Sector 4 Sheet 2 of 2
- 20-074 P4230 -Foul Water Longsections Sheet 1 of 2 Sector 4
- 20-074 P4231 -Foul Water Longsections Sheet 2 of 2 Sector 4
- 20-074 P4300 Proposed Watermain Layout Sector 4 Sheet 1 of 2
- 20-074 P4301 Proposed Watermain Layout Sector 4 Sheet 2 of 2

Additional Comments

The design submission will be subject to further technical review at connection application stage.

Irish Water cannot guarantee that its Network in any location will have the capacity to deliver a particular flow rate and associated residual pressure to meet the requirements of the relevant Fire Authority, see Section 1.17 of Water Code of Practice.

For further information, visit www.water.ie/connections

<u>Notwithstanding any matters listed above, the Customer (including any appointed</u> <u>designers/contractors, etc.) is entirely responsible for the design and construction of the Self-Lay</u> <u>Works.</u> Acceptance of the Design Submission by Irish Water will not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works. Appendix D Paved Area Factors

> 40 Engineering Assessment Report Project Number: 20-074 Document Reference: 20-074r.4001



Project :	Church Fields East
WM Ref:	20-074
Title:	Paved Area Factors
Date	Apr-23

Drainage Network Element

Roof SuDS(m ²)	2338
Roof Gully (m²)	3109
Green Roof (m²)	1800
Roads SuDS (m ²)	3363
Roads Gully (m²)	6218
Permeable Paving (m ²)	2970
Grass (m²)	25610
Total Drained Area of New Development (m ²)	<u>45408</u>

Paved Area Factors (PIMP Factors)

Roof SuDS	=	0.60
Roof Gully	=	0.95
Green Roof	=	0.60
Roads SuDS	=	0.90
Roads Gully	=	0.90
Permeable Paving	=	0.95
Grass	=	0.05

PIMP factor for Site 4

Element		
Roof SuDS	3.1%	
Roof Gully	6.5%	
Green Roof	2.4%	
Roads SuDS	6.7%	
Roads Gully	12.3%	
Permeable Paving	6.2%	
Grass	2.8%	
Average PIMP Factor Per site	<u>40.0%</u>	
Impermeable Area ha	<u>1.82</u>	ha

Greenfield Outflow

Total Allowed based on 3.7litres/second/hectare

4)
54

11)	waterman
	moguari

Project :	Church Fields East
WM Ref:	20-074
Title:	Paved Area Factors
Date:	Apr-23

Attenuation Tank Element

Roof SuDS(m²)	2338
Roof Gully (m²)	3109
Green Roof (m²)	1800
Roads SuDS (m ²)	3363
Roads Gully (m ²)	6218
Permeable Paving (m ²)	2970
Grass (m²)	25610
Total Drained Area of New Development (m ²)	<u>45408</u>

Paved Area Factors (PIMP Factors)

Roof SuDS	=	0.95
Roof Gully	=	0.95
Green Roof	=	0.95
Roads SuDS	=	0.90
Roads Gully	=	0.90
Permeable Paving	=	0.95
Grass	=	0.05

PIMP factor for Site 4

Element		
Roof SuDS	4.9%	
Roof Gully	6.5%	
Green Roof	3.8%	
Roads SuDS	6.7%	
Roads Gully	12.3%	
Permeable Paving	6.2%	
Grass	2.8%	
Average PIMP Factor Per site	<u>43.2%</u>	(Attenuation Check)
Impermeable Area ha	1.96	ha

Greenfield Outflow

Total Allowed based on 3.7litres/second/hectare

Qbar allowed ouflow for Total Area (I/s)	<u>16.80</u>
QBar formula	3.7x(4.71)
Site Area (Ha)	4.54

Appendix E Surface Water Pipe Design

> 41 Engineering Assessment Report Project Number: 20-074 Document Reference: 20-074r.4001

about:blank

Met Ei	.reann					
Return Period Rainfall D	epths t	for sli	ding Dura	ations		
Location - Damastown -	Irish (Grid:	Easting:	306642,	Northing:	241431,

	Inter	val						Years								
DURATION	6months,	1year,	2,	3,	4,	5,	10,	20,	30,	50,	75,	100,	150,	200,	250,	500,
5 mins	2.6,	3.6,	4.2,	5.0,	5.6,	6.0,	7.5,	9.1,	10.2,	11.7,	13.1,	14.1,	15.7,	17.0,	18.0,	N/A ,
10 mins	3.6,	5.0,	5.8,	7.0,	7.8,	8.4,	10.4,	12.7,	14.2,	16.3,	18.2,	19.7,	21.9,	23.7,	25.1,	N/A,
15 mins	4.2,	5.9,	6.9,	8.2,	9.2,	9.9,	12.3,	14.9,	16.7,	19.2,	21.4,	23.1,	25.8,	27.8,	29.5,	N/A ,
30 mins	5.6,	7.7,	8.9,	10.6,	11.8,	12.6,	15.5,	18.8,	20.9,	23.9,	26.6,	28.6,	31.8,	34.2,	36.2,	N/A ,
1 hours	7.4,	10.1,	11.5,	13.6,	15.1,	16.2,	19.7,	23.6,	26.2,	29.8,	32.9,	35.4,	39.1,	41.9,	44.3,	N/A ,
2 hours	9.7,	13.2,	14.9,	17.6,	19.3,	20.7,	25.0,	29.7,	32.8,	37.1,	40.9,	43.7,	48.1,	51.5,	54.3,	N/A ,
3 hours	11.5,	15.4,	17.4,	20.4,	22.3,	23.9,	28.7,	34.0,	37.4,	42.2,	46.3,	49.5,	54.3,	58.0,	61.1,	N/A,
4 hours	12.9,	17.2,	19.4,	22.6,	24.8,	26.4,	31.7,	37.4,	41.1,	46.2,	50.7,	54.1,	59.2,	63.2,	66.4,	N/A ,
6 hours	15.2,	20.0,	22.6,	26.2,	28.6,	30.5,	36.4,	42.8,	46.9,	52.5,	57.5,	61.2,	66.9,	71.2,	74.8,	N/A ,
9 hours	17.8,	23.4,	26.3,	30.4,	33.1,	35.2,	41.8,	48.9,	53.5,	59.7,	65.2,	69.3,	75.6,	80.3,	84.2,	N/A,
12 hours	20.0,	26.1,	29.3,	33.8,	36.7,	39.0,	46.1,	53.8,	58.7,	65.4,	71.3,	75.7,	82.4,	87.4,	91.6,	N/A ,
18 hours	23.6,	30.5,	34.1,	39.2,	42.5,	45.0,	53.0,	61.5,	67.0,	74.4,	80.8,	85.7,	93.0,	98.6,	103.1,	N/A,
24 hours	26.5,	34.1,	37.9,	43.5,	47.1,	49.8,	58.4,	67.7,	73.5,	81.5,	88.4,	93.6,	101.4,	107.3,	112.2,	128.6,
2 days	32.9,	41.6,	45.9,	52.1,	56.1,	59.1,	68.5,	78.4,	84.7,	93.2,	100.4,	105.9,	114.0,	120.2,	125.2,	142.1,
3 days	38.1,	47.6,	52.4,	59.0,	63.3,	66.6,	76.6,	87.2,	93.8,	102.7,	110.4,	116.1,	124.6,	131.0,	136.2,	153.6,
4 days	42.7,	52.9,	58.0,	65.1,	69.7,	73.1,	83.7,	94.8,	101.8,	111.1,	119.1,	125.0,	133.8,	140.5,	145.8,	163.8,
6 days	50.7,	62.2,	67.8,	75.7,	80.7,	84.4,	96.0,	108.1,	115.6,	125.7,	134.2,	140.5,	149.9,	157.0,	162.6,	181.6,
8 days	57.8,	70.3,	76.4,	84.9,	90.3,	94.4,	106.8,	119.7,	127.7,	138.3,	147.3,	154.0,	163.9,	171.3,	177.3,	197.1,
10 days	64.3,	77.7,	84.3,	93.4,	99.1,	103.4,	116.6,	130.2,	138.6,	149.8,	159.2,	166.2,	176.6,	184.3,	190.5,	211.1,
12 days	70.3,	84.7,	91.6,	101.2,	107.3,	111.8,	125.7,	139.9,	148.7,	160.4,	170.2,	177.5,	188.3,	196.3,	202.7,	224.1,
16 days	81.6,	97.5,	105.1,	115.6,	122.3,	127.2,	142.3,	157.7,	167.2,	179.7,	190.3,	198.1,	209.6,	218.1,	224.9,	247.6,
20 days	92.0,	109.3,	117.5,	128.9,	136.0,	141.3,	157.5,	173.9,	184.0,	197.3,	208.5,	216.7,	228.9,	237.9,	245.1,	268.9,
25 days	104.3,	123.0,	132.0,	144.2,	152.0,	157.7,	175.0,	192.7,	203.4,	217.6,	229.5,	238.2,	251.1,	260.6,	268.2,	293.3,
NOTES:																

N/A Data not available

These values are derived from a Depth Duration Frequency (DDF) Model

For details refer to:

'Fitzgerald D. L. (2007), Estimates of Point Rainfall Frequencies, Technical Note No. 61, Met Eireann, Dublin', Available for download at www.met.ie/climate/dataproducts/Estimation-of-Point-Rainfall-Frequencies_TN61.pdf

Planter Vol = $(2.3x1.1x0.90) = 2.28 \text{ m}^3$

 $\begin{array}{ll} \text{M5 60} &= 16.2 \\ \text{M5 2day} &= 59.1 \\ \text{Ratio} &= 0.27 \end{array} \\ \begin{array}{ll} \text{Roof Area} &= 35 \text{ m}^2 \\ \text{Req Vol} &= (35 \text{x} 10^{-3}) \text{x} 25 \\ \text{Req Vol} &= 0.875 \text{m}^3 = 0.88 \text{m}^3 \\ \text{Voids} &= 40\% \\ \text{Req Vol Soil} &= (0.88/0.40) = 2.2 \text{ m}^3 \end{array}$



Page 1 20-074 Church Fields Church Field East Surface water - 5 Years

Design Settings

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	5	Maximum Rainfall (mm/hr)	50.0
Additional Flow (%)	0	Minimum Velocity (m/s)	1.00
FSR Region	Scotland and Ireland	Connection Type	Level Soffits
M5-60 (mm)	16.800	Minimum Backdrop Height (m)	0.600
Ratio-R	0.270	Preferred Cover Depth (m)	1.200
CV	0.750	Include Intermediate Ground	\checkmark
Time of Entry (mins)	4.00	Enforce best practice design rules	\checkmark

<u>Nodes</u>

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
S1	0.047	4.00	83.600	1200	707002.750	741581.052	1.758
S2			82.871	1200	706966.243	741577.809	1.494
S3	0.070	4.00	84.895	1200	707030.758	741535.520	1.961
S4	0.269	4.00	85.950	1200	707067.617	741539.250	1.425
S5	0.075	4.00	85.125	1200	707033.883	741503.733	2.356
S6	0.049	4.00	84.895	1200	707037.139	741469.373	2.291
S7	0.065	4.00	84.000	1200	706999.405	741465.917	1.735
S8	0.010	4.00	84.595	1350	707041.289	741426.286	2.584
S9	0.040	4.00	84.147	1350	707020.716	741424.719	2.315
S10	0.006	4.00	83.405	1500	706987.471	741433.762	2.283
S11			83.250	1500	706999.064	741447.003	2.415
S12			83.250	1800	706986.000	741442.290	2.488
SW- A3 MH5			83.130	1500	706976.090	741438.432	2.430
S14	0.029	4.00	85.947	1350	707091.128	741431.216	2.232
S15	0.029	4.00	86.430	1350	707097.089	741435.548	2.677
S16	0.052	4.00	86.760	1200	707092.789	741484.068	2.762
S17	0.200	4.00	86.450	1200	707087.404	741543.902	2.160
S18	0.024	4.00	86.000	1200	707085.274	741567.903	1.580
S19	0.210	4.00	86.200	1200	707149.519	741574.057	1.350
SW-A3 MH1			82.690	1200	706967.121	741560.524	1.400
S20			83.185	1200	706974.684	741430.850	2.014
S21	0.086	4.00	83.325	1200	706975.763	741414.579	2.072
S22	0.036	4.00	83.135	1200	706966.883	741382.051	1.713
S23	0.059	4.00	83.060	1200	706961.848	741372.932	1.585
S24	0.037	4.00	82.760	1200	706954.232	741342.633	1.132
S25	0.007	4.00	82.960	1200	706967.987	741339.226	1.261
S26	0.053	4.00	82.990	1200	706965.439	741328.885	1.238
S27	0.151	4.00	84.200	1200	707029.945	741369.559	1.640
S28	0.116	4.00	84.025	1350	707026.009	741358.768	1.388
S29	0.025	4.00	83.750	1200	707008.177	741328.688	1.419
S30		4.00	83.395	1200	706959.541	741306.447	1.425
S31	0.211	4.00	84.468	1200	707042.262	741416.181	2.251
1		4.00	84.575	1200	707029.181	741552.408	1.425
SW-2.1		4.00	84.670	1200	707040.123	741436.991	1.425
SW-2.2			83.613	1500	707000.979	741430.063	2.689
SW-2.3			83.367	1500	707002.804	741436.783	2.501

				Waterman M	oylan Consult	ting	File: 4A with	foul R.0	2.pfd	Page	e 2			
					1	Network: Sto	orm Net	work	20-0	20-074 Church Fields				
9	AUSI						Sidharth Kur	ella		Chu	Church Field East			
							2023-03-20			Surf	ace wate	r - 5 Years		
						<u>Link</u>								
	Name	US	DS	Length	ks (mm) /	US II	DS IL	Fall	Slope	Dia	T of C	Rain		
		Node	Node	(m)	n	(m)	(m)	(m)	(1:X)	(mm)	(mins)	(mm/hr)		
	1.011	S12	SW- A3 N	1H5 <u>10.63</u> 4	0.600	80.76	80.700	0.062	171.5	525	8.44	50.0		
	1.009	S11	S12	8.128	0.600	80.83	5 80.762	0.073	111.3	450	8.34	50.0		
	1.007	S9	SW-2.2	20.448	0.600	81.83	2 81.730	0.102	200.0	450	8.06	50.0		
	4.007	S10	SW-2.2	9.632	0.600	81.12	2 81.074	0.048	200.7	300	6.74	50.0		
	6.006	S20	S10	9.737	0.600	81.17	1 81.122	0.049	198.7	300	6.60	50.0		
	6.005	S21	S20	16.307	0.600	81.25	3 81.171	0.082	198.9	300	6.45	50.0		
	6.004	S22	S21	33.718	0.600	81.42	2 81.253	0.169	199.5	225	6.21	50.0		
	6.003	S23	S22	10.416	0.600	81.47	5 81.422	0.053	196.5	225	5.60	50.0		
	6.002	S24	S23	30.647	0.600	81.62	8 81.475	0.153	200.3	225	5.41	50.0		
	6.001	S25	S24	14.170	0.600	81.69	9 81.628	0.071	199.6	225	4.86	50.0		
	7.001	S26	S25	10.650	0.600	81.75	2 81.699	0.053	200.9	225	4.60	50.0		
	4.000	S29	S25	41.549	0.600	82.33	1 81.699	0.632	65.7	225	4.43	50.0		
	7.000	S30	S26	28.070	0.600	81.97	0 81.752	0.218	128.8	225	4.41	50.0		
	1.006	S8	S9	20.447	0.600	82.01	1 81.832	0.179	114.2	450	7.82	50.0		
	5.004	S7	S11	18.211	0.600	82.26	5 81.658	0.607	30.0	300	5.77	50.0		
	5.002	S31	S8	10.136	0.600	82.21	7 82.161	0.056	181.0	300	5.15	50.0		
	1.005	S14	S8	49.915	0.600	83.71	.5 83.020	0.695	71.8	300	7.65	50.0		
	1.004	S15	S14	7.505	0.600	83.75	3 83.715	0.038	197.5	300	7.20	50.0		
	1.003	S16	S15	48.710	0.600	83.99	8 83.753	0.245	198.8	300	7.09	50.0		
	1.002	S17	S16	58.113	0.600	84.29	0 83.998	0.292	199.0	300	6.35	50.0		
	1.001	S18	S17	26.058	0.600	84.42	0 84.290	0.130	200.4	225	5.48	50.0		
	1.000	S19	S18	64.539	0.600	84.85	0 84.420	0.430	150.1	225	5.01	50.0		
	5.001	S27	S31	48.222	0.600	82.56	0 82.292	0.268	179.9	225	5.01	50.0		
	5.000	S28	S27	11.486	0.600	82.63	7 82.560	0.077	149.2	225	4.18	50.0		

Nan	ne Vo	el	Сар	Flow	US	DS	Σ Area	Σ Add	Pro	Pro
	(m	/s)	(I/s)	(I/s)	Depth	Depth	(ha)	Inflow	Depth	Velocity
					(m)	(m)		(I/s)	(mm)	(m/s)
1.01	1.7	07	369.5	258.7	1.963	1.905	1.909	0.0	325	1.840
1.00	9 1.9	26	306.3	258.7	1.965	2.038	1.909	0.0	319	2.147
1.00	1.4	34	228.0	145.3	1.865	1.433	1.072	0.0	261	1.516
4.00	07 1.1	06	78.2	41.9	1.983	2.239	0.309	0.0	156	1.124
6.00	<mark>)6</mark> 1.1	11	78.6	41.1	1.714	1.983	0.303	0.0	154	1.123
6.00)5 1.1	11	78.5	41.1	1.772	1.714	0.303	0.0	154	1.122
6.00	0.9	22	36.7	29.4	1.488	1.847	0.217	0.0	153	1.022
6.00	0.9	29	36.9	24.5	1.360	1.488	0.181	0.0	134	0.992
6.00	0.9	20	36.6	16.5	0.907	1.360	0.122	0.0	106	0.897
6.00	0.9	22	36.6	11.5	1.036	0.907	0.085	0.0	87	0.818
7.00	0.9	18	36.5	7.2	1.013	1.036	0.053	0.0	67	0.715
4.00	0 1.6	15	64.2	3.4	1.194	1.036	0.025	0.0	35	0.859
7.00	0 1.1	50	45.7	0.0	1.200	1.013	0.000	0.0	0	0.000
1.00) <mark>6</mark> 1.9	01	302.4	139.9	2.134	1.865	1.032	0.0	215	1.866
5.00	2.8	81	203.6	71.6	1.435	1.292	0.528	0.0	123	2.638
5.00	1.1	65	82.4	64.8	1.951	2.134	0.478	0.0	201	1.286
1.00)5 1.8	57	131.3	73.7	1.932	1.275	0.544	0.0	161	1.909
1.00)4 1.1	15	78.8	69.8	2.377	1.932	0.515	0.0	221	1.253
1.00)3 1.1	11	78.5	65.9	2.462	2.377	0.486	0.0	211	1.240
1.00	1.1	11	78.5	58.8	1.860	2.462	0.434	0.0	194	1.215
1.00	0.9	20	36.6	31.7	1.355	1.935	0.234	0.0	162	1.032
1.00	0 1.0	65	42.3	28.5	1.125	1.355	0.210	0.0	135	1.139
5.00	0.9	71	38.6	36.2	1.415	1.951	0.267	0.0	174	1.100
5.00	0 1.0	68	42.5	15.7	1.163	1.415	0.116	0.0	94	0.989

C,	AUS	EV		~ { }	Wate	rman M	oylan Co	onsulting	g File: 4 Netw Sidha 2023	IA with fo ork: Stori rth Kurel 03-20	oul R.02 m Netw la	.pfd ork	Page 3 20-07 Churc Surfac	3 4 Church h Field Ea ce water -	Fields ast - 5 Years	
									LINKS							
	Name	N	US Iode	E No	DS ode	Lengt (m)	h ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)	
	2.003	S5	oue	S6		32.96	9	0.600	82.769	82.604	0.165	199.8	300	5.24	50.0	
	5.003	S6		S7		37.89	2	0.600	82.604	82.265	0.339	111.8	300	5.66	50.0	
	2.002	S3		S5		33.07	8	0.600	82.934	82.769	0.165	200.5	300	4.74	50.0	
	7.001	1 S2		SW-A	3 MH1	17.30	7	0.600	81.377	81.290	0.087	198.9	225	4.73	50.0	
	3.000	S4		S3		34.16	3	0.600	84.525	83.457	1.068	32.0	225	4.25	50.0	
	7.000	1 S1		S2		36.65	1	0.600	81.842	81.377	0.465	78.8	225	4.41	50.0	
	7.000	2 1		S 3		16.96	1	0.600	83.150	83.009	0.141	120.0	225	4.24	50.0	
	3.000_	1 SV	V-2.1	S8		10.76	8	0.600	83.245	83.064	0.181	59.5	225	4.11	50.0	
	1.008 1.009_	SV 1 SV	V-2.2 V-2.3	SW-2 S11	.3	11.54 6.15	2 7	0.600 0.600	80.924 80.866	80.866 80.835	0.058 0.031	199.0 198.6	450 450	8.20 8.27	50.0 50.0	
			Na	me	Vel	Can	Flow	115	DS	Σ Δrea	Σ Δά	d Pro	D	ro		
			ING	ine	(m/s)	(1/s)	(1/s)	Depth	Depth	(ha)	Inflo	w Dent	h Velo	ncity		
					(11, 5)	(1/3)	(1/3)	(m)	(m)	(na)	(1/s)	(mm) (m	/s)		
			2.00)3	1.108	78.3	56.1	2.056	1.991	0.414	0.	0 18	, (8 1	.202		
			5.00)3	1.486	105.1	62.7	1.991	1.435	0.463	0.	0 16	- 71	.550		
			2.00)2	1.107	78.2	45.9	1.661	2.056	0.339	0.	0 16	6 1	.150		
			7.00)1 1	0.923	36.7	6.4	1.269	1.175	0.047	0.	0 6	3 0	.693		
			3.00	00	2.321	92.3	36.5	1.200	1.213	0.269	0.	0 9	82	.187		
			7.00	00 1	1.474	58.6	6.4	1.533	1.269	0.047	0.	0 5	0 0	.970		
			7.00	0 2	1.192	47.4	0.0	1.200	1.661	0.000	0.	0	0 0	.000		
			3.00	00_1	1.698	67.5	0.0	1.200	1.306	0.000	0.	0	0 0	.000		
			1.00	18	1 437	228.6	187 2	2 239	2 051	1 381	0	0 31	2 1	596		
			1.00)9_1	1.439	228.8	187.2	2.051	1.965	1.381	0.	0 31	1 1	.596		
								<u>Pipelin</u>	<u>ne Schedu</u>	<u>lle</u>						
		Link	Len	gth S	Slope	Dia	Link	US C	L USI	L US D	Depth	DS CL	DS IL	DS De	pth	
			(n	n) ((1:X)	(mm)	Туре	(m)	(m)) (ı	m)	(m)	(m)	(m)		
		1.011	10.	634 1	L71.5	525	Circula	r 83.25	50 80.70	52	1.963	83.130	80.700	1.9	905	
		1.009	8.	128 1	L11.3	450	Circula	r 83.25	50 80.83	35	1.965	83.250	80.762	2.0	038	
		1.007	20.4	448 2	200.0	450	Circula	r 84.14	17 81.83	32	1.865	83.613	81.730	1.4	433	
		4.007	9.0	632 2	200.7	300	Circula	r 83.40	05 81.12	22	1.983	83.613	81.074	2.2	239	
		6.006	9.	737 1	L98.7	300	Circula	r 83.18	85 81.1	71	1.714	83.405	81.122	1.9	983	
		6.005	16.3	307 1	L98.9	300	Circula	r 83.32	25 81.2	53	1.772	83.185	81.171	1.7	714	
		6.004	33.	718 1	199.5	225	Circula	r 83.13	85 81.42	22	1.488	83.325	81.253	1.8	347	
		6.003	10.4	416 1	196.5	225	Circula	r 83.06	50 81.4	75	1.360	83.135	81.422	1.4	488	
		6.002	30.0	647 2	200.3	225	Circula	r 82.76	50 81.62	28	0.907	83.060	81.475	1.3	360	
			Link	US	Dia	No	de	МН		DS	Dia	Node	!	МН		
				Node	(mm	і) Ту	ре	Туре	N	ode	(mm)	Туре	-	Гуре		
		1	.011	S12	180	0 Mar	hole	Adoptab	le SW-	A3 MH5	1500	Manho	le Ado	optable		
		1	.009	S11	150	0 Mar	hole	Adoptab	le S12	-	1800	Manho	le Ado	optable		
		1	1.007	S9	135	0 Mar	hole	Adoptab	le SW-2	2.2	1500	Manho	le Ado	optable		
		4	1.007	510	150	u Mar	inole	Adoptab	ie SW-2		1500	Manho	e Ado	optable		
		6	0.006	520	120	U Mar	inole	Adoptab	e 510		1500	Nanho	e Ado	optable		
		e	0.005	521	120	v iviar		Adoptab	10 S20		1200	ivianno	ne Ado			
		6	0.004	52Z	120			Adoptabl			1200	Manho	de Ade			
		t c	0.003	3∠3 <24	120		holo	Adoptabl	C 322		1200	IVIdf1f10	ne Add	optable		
		e	0.002	524	120		nole	հսօրւզը	JZ3		1200	ivid(1110	He Add	pranie		

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			Wate	rman M	loylan Cor	nsulting	File: 4A wi	ith foul R.02.	pfd	Page 4	
СЛИ							Network:	Storm Netwo	ork	20-074	Church Fields
CAUS							Sidharth K	Curella		Church	Field East
							2023-03-2	0		Surface	water - 5 Years
						Pipeline S	Schedule				
	Link	Length	Slope	Dia	Link	US CL	USIL	US Depth	DS CL	DS IL	DS Depth
	6.004	(m)	(1:X)	(mm)	Туре	(m)	(m)	(m)	(m)	(m)	(m)
	6.001	14.170	199.6	225	Circulai	82.960	81.699	1.036	82.760	81.628	0.907
	7.001	10.650	200.9	225	Circulai	82.990	81.752	1.013	82.960	81.699	1.036
	4.000	41.549	65.7 120.0	225	Circular	6 83.750	82.331	1.194	82.960	81.699	1.036
	7.000	28.070	128.8	225	Circular	6 83.395	81.970	1.200	82.990	81.752	1.013
	1.006	20.447	114.2	450	Circular	84.595	82.011	2.134	84.147	81.832	1.805
	5.004	18.211	30.0	300	Circular	84.000	82.205	1.435	83.250	81.058	1.292
	5.002	10.136	181.0	300	Circular		82.217	1.951	84.595	82.101	2.134
	1.005	49.915	/1.8 107 F	300	Circular	65.947	03./15	1.932	84.595	83.020	1.275
	1.004	7.505	197.5	300	Circular	00.430	03./33	2.377	85.947	03./13	1.932
	1.005	40.710	190.0	200	Circular		03.990	1 960	00.450 06 760	03./33	2.377
	1.002	26.113	199.0	300	Circular		84.290	1.800	80.700 96.4E0	83.998	2.402
	1.001	20.058	200.4	225	Circular		84.420	1.355	80.450	84.290	1.935
	1.000	04.559	170.0	225	Circular	80.200	84.85U	1.125	80.000	84.420	1.355
	5.001	40.222	1/9.9	225	Circular	84.200	82.500	1.415	84.408	82.292	1.951
	5.000	11.460	149.2	225	Circular		82.037	1.103	84.200	82.500	1.415
	2.003	32.909	199.8	300	Circular	01 00E	82.709 93.604	2.050	84.895 84.000	82.004	1.991
	2.002	27.032	111.0 200 E	200	Circular	04.095	02.004	1.991	04.000 0E 10E	02.205	1.455
	2.002	33.076 17 207	200.5	200	Circular	04.095 07 071	02.954	1.001	03.123	02.709	2.050
	2.000	2/ 162	22.0	225	Circular		01.377	1.209	02.090 01 005	01.290	1.175
	7 000 1	26 651	52.0 70 0	225	Circular	00.900 00.900	04.525	1.200	04.095 07 071	05.457	1.215
	7.000_1	16.061	120.0	225	Circular		01.042	1.555	02.071 04 00E	01.577	1.209
	3.000 1	10.768	59.5	225	Circular	84.575	83.245	1.200	84.893 84.595	83.064	1.306
	1 008	11 542	199 0	450	Circula	83 613	80 924	2 239	83 367	80 866	2 051
	1:				Nodo	NALL	0010-1	Dia	Nod		
	LIN		he (m	ia m)	Type	Type	Nod	o Dia le (mm) Typ	e 9 1	
	6 001	\$25	12 12	200 N	1anhole	Adontabl	e \$24	1200	Manh	ole Ado	ontable
	7 001	525	10		lanhole	Adoptabl	• \$25	1200	Manh		ntable
	4 000	520	12	200 N	lanhole	Adoptabl	e S25	1200	Manh	ole Add	optable
	7 000	S30	12	200 N	Ianhole	Adoptabl	e 526	1200	Manh	ole Add	optable
	1.006	58	13	350 N	lanhole	Adoptabl	e 59	1350) Manh	ole Add	optable
	5.004	S7	12	200 N	lanhole	Adoptabl	e S11	1500) Manh	ole Add	potable
	5.002	S31	12	200 N	lanhole	Adoptabl	e S8	1350	Manh	ole Ado	optable
	1.005	S14	13	350 N	lanhole	Adoptabl	e S8	1350) Manh	ole Ado	optable
	1.004	S15	13	350 N	Ianhole	Adoptabl	e S14	1350) Manh	ole Ado	ptable
	1.003	S16	12	200 N	lanhole	Adoptabl	e S15	1350) Manh	ole Ado	ptable
	1.002	S17	12	200 N	lanhole	Adoptabl	e S16	1200) Manh	ole Ado	optable
	1.001	S18	12	200 N	1anhole	Adoptabl	e S17	1200) Manh	ole Ado	optable
	1.000	S19	12	200 N	1anhole	Adoptabl	e S18	1200) Manh	ole Ado	ptable
	5.001	S27	12	200 N	1anhole	Adoptabl	e S31	1200) Manh	ole Add	ptable
	5.000	S28	13	350 N	1anhole	Adoptabl	e S27	1200) Manh	ole Add	ptable
	2.003	S5	12	200 N	Ianhole	Adoptabl	e S6	1200) Manh	ole Add	optable
	5.003	S6	12	200 N	Ianhole	Adoptabl	e S7	1200) Manh	ole Add	ptable
	2.002	S3	12	200 N	lanhole	Adoptabl	e S5	1200) Manh	ole Add	optable
	7.001	_1 S2	12	200 N	lanhole	Adoptabl	e SW-A3	MH1 1200) Manh	ole Add	optable
	3.000	S4	12	200 N	lanhole	Adoptabl	e S3	1200) Manh	ole Add	optable
	7.000	_1 S1	12	200 N	lanhole	Adoptabl	e S2	1200) Manh	ole Add	optable
	7.000	_2 1	12	200 N	lanhole	Adoptabl	e S3	1200) Manh	ole Add	optable
	3.000	_1 SW-3	2.1 12	200 N	lanhole	Adoptabl	e S8	1350) Manh	ole Ado	optable
	1.008	SW-	2.2 1	500 M	lanhole	Adoptabl	e SW-2.3	1500) Manh	ole Ado	optable
	_,	5		•		I	2.1. 2.0	2000			

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USEV		Vaterman			Netwo Sidhart 2023-0	rk: Storm Netv th Kurella 13-20		20-074 Church Fields Church Field East Surface water - 5 Years			
				<u>Pipeline </u>	Schedul	<u>e</u>					
Link 1.009	Length (m) 1 6.157	Slope Di (1:X) (mr 198.6 4	a Link n) Type 50 Circular	US CL (m) 83.367	US I (m) 80.86	L US Depth (m) 56 2.051	D 83	S CL (m) 3.250	DS IL DS (m) 80.835	Depth (m) 1.965	
	Link	US Dia Node (mn SW-2.3 150	a Node n) Type 0 Manhol	M Typ e Adopt	H De l table S	DS Dia Node (mm) 511 1500	N T Ma	i ode ype inhole	MH Type Adoptable		
			<u> </u>	Manhole	Schedul	e					
Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connection	าร	Link	IL (m)	Dia (mm)	
S1	707002.750	741581.05	2 83.600	1.758	1200	₀ ←					
62	700000 242	744577.00	0 00 074	4 40 4	4200		0	7.000	1 81.842	225	
52	706966.243	/415//.80	9 82.871	1.494	1200	— 1	1	7.000_	_1 81.377	225	
						0	0	7.001_	_1 81.377	225	
S3	707030.758	741535.52	0 84.895	1.961	1200	1	1 2	7.000_ 3.000	2 83.009 83.457	225 225	
54	707067 617	7/1520.25	0 85 050	1 / 25	1200	0	0	2.002	82.934	300	
54	/0/00/.01/	741339.23	0 85.950	1.425	1200	0 <					
65	707022.002	741502 72	2 05 125	2 250	1200	1	0	3.000	84.525	225	
35	707033.883	741503.73	3 85.125	2.350	1200	\oint	T	2.002	82.769	300	
56	707037 139	741469 37	2 84 895	2 291	1200	1	0	2.003	82.769	300	
50	/0/03/.135	741403.37	5 04.055	2.291	1200	0 <	Ţ	2.005	02.004	500	
\$7	706999 /05	7/1/65 01	7 8/ 000	1 735	1200		0	5.003	82.604	300	
57	700333.403	741403.31	.7 84.000	1.755	1200		T	5.005	82.205	500	
0	707041 200	7/1/26 20	6 94 505	2 5 0 1	1250	0 1	0	5.004	82.265	300	
20	707041.285	741420.20	0 04.353	2.364	1330	0 ← → 3	2 3	5.000_ 5.002 1.005	82.161 83.020	300 300	
59	707020 716	741424 71	9 84 147	2 3 1 5	1350	2	0	1.006	82.011	450	
55	, 0, 020.710	, 41424./J		2.313	100	0 <	T	1.000	01.032	750	
C10	706007 474	7/1/22 70	C 03 40F	2 202	1500		0	1.007	81.832	450	
210	/098/.4/1	/41433./6	02 83.405	2.283	1200	1	T	0.006	81.122	300	
							0	4.007	81.122	300	



Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connection	IS	Link	IL (m)	Dia (mm)
S11	706999.064	741447.003	83.250	2.415	1500	1	1	5.004	81.658	300
							2	1.009_1	80.835	450
						2	0	1 009	80 835	450
S12	706986.000	741442.290	83.250	2.488	1800		1	1.009	80.762	450
						0 1				
							0	1.011	80.762	525
SW- A3 MH5	706976.090	741438.432	83.130	2.430	1500	\mathcal{G}^{1}	1	1.011	80.700	525
S14	707091.128	741431.216	85.947	2.232	1350	o <	1	1.004	83.715	300
							0	1.005	83.715	300
S15	707097.089	741435.548	86.430	2.677	1350		1	1.003	83.753	300
						0 "	0	1.004	83.753	300
S16	707092.789	741484.068	86.760	2.762	1200		1	1.002	83.998	300
							0	1.003	83.998	300
S17	707087.404	741543.902	86.450	2.160	1200		1	1.001	84.290	225
						0	0	1.002	84.290	300
S18	707085.274	741567.903	86.000	1.580	1200	-1	1	1.000	84.420	225
<u></u>	707140 510	741574 057	00.000	1 250	1200	ŏ	0	1.001	84.420	225
213	707149.519	741574.057	80.200	1.350	1200	₀ ←				
							0	1.000	84.850	225
SW-A3 MH1	706967.121	741560.524	82.690	1.400	1200		1	7.001_1	81.290	225
S20	706974.684	741430.850	83.185	2.014	1200	∂ →0	1	6.005	81.171	300
						1	0	6.006	81.171	300
S21	706975.763	741414.579	83.325	2.072	1200	● ●	1	6.004	81.253	225
						/ 1	0	6.005	81.253	300
S22	706966.883	741382.051	83.135	1.713	1200	, second	1	6.003	81.422	225
						1	0	6.004	81.422	225


Waterman Moylan Consulting	File: 4A with foul R.02.pfd	Page 7
	Network: Storm Network	20-074 Church Fields
	Sidharth Kurella	Church Field East
	2023-03-20	Surface water - 5 Years

Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	5	Link	IL (m)	Dia (mm)
S23	706961.848	741372.932	83.060	1.585	1200	ϕ	1	6.002	81.475	225
						1	0	6.003	81.475	225
524	/06954.232	/41342.633	82.760	1.132	1200		1	6.001	81.628	225
							0	6.002	81.628	225
S25	706967.987	741339.226	82.960	1.261	1200		1	7.001	81.699	225
						0 ~ ~ ~ 2	2	4.000	81.699	225
526	700005 420	741220.005	02.000	1 2 2 0	1200	1	1	5.001	81.699	225
526	706965.439	741328.885	82.990	1.238	1200	\oint	1	7.000	81.752	225
						1	0	7.001	81.752	225
S27	707029.945	741369.559	84.200	1.640	1200	\oint	1	5.000	82.560	225
						1′	0	5.001	82.560	225
S28	707026.009	741358.768	84.025	1.388	1350	Š				
							0	5.000	82.637	225
S29	707008.177	741328.688	83.750	1.419	1200	0 <	0	4.000	02 221	225
620	700000 0 44	744206 447	02.205	4 425	1200		0	4.000	82.331	225
530	706959.541	741306.447	83.395	1.425	1200	Ċ	0	7.000	91 070	225
C21	707042 262	7/1/16 101	01 160	2 251	1200	0	1	7.000	81.970	225
331	707042.202	741410.181	04.400	2.231	1200	$\hat{\phi}$	1	5.001	02.232	220
1	707020 404	744552 400	04 575	4 425	1200	1	0	5.002	82.217	300
I	707029.181	741552.408	84.575	1.425	1200	\bigcirc	0	7.000 2	83.150	225
SW-2.1	707040.123	741436.991	84.670	1.425	1200					
						\bigcirc	0	2 000 1	92 J/E	225
5\// 2.2	707000 070	7/1/20 062	82 612	2 600	1500	0 0	1	3.000_1	03.243 81.074	225
300-2.2	707000.979	741430.003	05.015	2.005	1300	12	2	1.007	81.730	450
							0	1.008	80.924	450
SW-2.3	707002.804	741436.783	83.367	2.501	1500		1	1.008	80.866	450
						1	0	1.009_1	80.866	450

CAUSEWAY 🛟	Waterman Moylan Consulting	File: 4A with foul R.02.pfd Network: Storm Network Sidharth Kurella 2023-03-20	Page 8 20-074 Church Fields Church Field East Surface water - 5 Years				
	Simulatio	n Settings					
Rainfall M N	ethodology FSR FSR Region Scotland and Irelan 15-60 (mm) 16.800 Ratio-R 0.270 Summer CV 0.750 Winter CV 0.840	Analysis SpeedDetailedandSkip Steady StatexDrain Down Time (mins)240Additional Storage (m³/ha)20.0Check Discharge Rate(s)xCheck Discharge Volumex					
15 60 30 120	Storm D 180 360 600 9 240 480 720 1	Purations 960 2160 4320 720 440 2880 5760 864	00 10080 40				
R	eturn Period Climate Change (years) (CC %) 5 20	Additional Area Additional Florence (A %) (Q %)	bw				
	Node S12 Online Hy	ydro-Brake [®] Control					
F Downstr Replaces Downstr Invert Design D Design	lap Valve x eam Link 1.011 eam Link √ Level (m) 80.762 Min Out pepth (m) 2.500 Min Node Flow (I/s) 16.8	Objective (HE) Minimise Sump Available √ Product Number CTL-SHE-0162 let Diameter (m) 0.225 e Diameter (mm) 1800	e upstream storage 2-1680-2500-1680				
	Node S11 Depth/Ar	ea Storage Structure					
Base Inf Coefficier Side Inf Coefficier	t (m/hr) 0.06300 Safety Fa t (m/hr) 0.06300 Porc	ctor 1.0 Invert osity 0.40 Time to half em	Level (m) 80.835 pty (mins) 0				
Depth / (m) 0.000 12	Area Inf Area Depth Ai m²) (m²) (m) (n LOO.O 0.O 1.765 110	rea Inf Area Depth Are n²) (m²) (m) (m² D0.0 0.0 1.766 0.	a Inf Area (m²) 0 1300.0				



Results for 5 year +20% CC Critical Storm Duration. Lowest mass balance: 99.71%

		US Nodo (Peak	Level	Depth	Inflow	Node	Flood	St	atus
15 minuto wintor	C1	Noue (10	(III) 91.006	0.064	10 /	0 1062		OK	
15 minute winter	51		10	01.900	0.004	10.4	0.1002	0.0000		
15 minute winter	52		10	81.401	0.084	75.2	0.0934	0.0000	OK	
15 minute winter	55		10	84 663	0.271	59.2	0.4550	0.0000	OK	
15 minute winter	55		10	83 073	0.138	873	0.0779	0.0000		HARGED
15 minute winter	55		11	87 843	0.304	95.5	0.3371	0.0000	OK	
15 minute winter	50		11	87 438	0.235	108.0	0.3720	0.0000	OK	
15 minute winter	58		11	82 327	0.175	190.8	0.3255	0.0000	OK	
15 minute winter	50		11	82 195	0.363	198.8	0.4705	0.0000	OK	
360 minute winter	S10		280	81 647	0.505	11 4	0.0447	0.0000	SURCI	HARGED
360 minute winter	S11		280	81.646	0.811	70.9	358.2812	0.0000	SURCI	HARGED
360 minute winter	\$12		280	81 646	0 884	39.2	2 2486	0 0000	SURCI	HARGED
15 minute summer	SW/	- A3 MH5	200	80 700	0.004	15.6	0 0000	0.0000	OK	
15 minute winter	S14		11	83 916	0.000	97.0	0.0000	0.0000	OK	
15 minute winter	S15		11	8/ 021	0.201	97.0	0.5400	0.0000	OK	
15 minute winter	S16		11	84 343	0.200	90.4	0.4415	0.0000	SURCI	HARGED
15 minute winter	S10 S17		11	84.545 84.667	0.345	90.4 94 7	1 12/19	0.0000	SURCI	
15 minute winter	S12		11	84.007	0.377	16 S	0.6360	0.0000	SURCI	
15 minute winter	S10		11	85 228	0.443	40.8	1 6021	0.0000	SURCI	
15 minute winter	S/W	A2 MH1	10	81 270	0.378	10.0	0.0000	0.0000	OK	HANGED
360 minute winter	570		280	81.570 81.647	0.080	10.2	0.0000	0.0000		
360 minute winter	S20		200	81.047 81.647	0.470	11.7	0.5580	0.0000	SURCI	
15 minute winter	\$22		11	81.047	0.394	39.6	0.7723	0.0000	SURCI	
15 minute winter	522		11	81.700 81.750	0.270	37.0	0.4303	0.0000	SURCI	
15 minute winter	525		11	01.755	0.204	57.0	0.5524	0.0000	501101	IANGLU
Link Event	JS	Link		DS	Outflo	w Velo	ocity Flov	v/Cap	Link	Discharge
Link Event (Upstream Depth) N	JS ode	Link		DS Node	Outflor (I/s)	w Velc (m	ocity Flov /s)	v/Cap V	Link ′ol (m³)	Discharge Vol (m ³)
Link Event (Upstream Depth) No. 15 minute winter S1	JS ode	Link 7.000_1	S2	DS Node	Outflo (I/s) 10	w Velc (m .4 0.	ocity Flov /s) .930	v/Cap V 0.177	Link 'ol (m³) 0.4178	Discharge Vol (m³)
Link Event (Upstream Depth) No. 15 minute winter S1 15 minute winter S2	JS ode	Link 7.000_1 7.001_1	S2 SV	DS Node /-A3 MH1	Outflor (I/s) 10.	w Velo (m .4 0.	ocity Flow /s) .930 .776	v/Cap V 0.177 0.278	Link /ol (m³) 0.4178 0.2274	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) No 15 minute winter S1 15 minute winter S2 15 minute winter S3	JS ode	Link 7.000_1 7.001_1 2.002	S2 SV S5	DS Node V-A3 MH1	Outflor (I/s) 10. 70.	w Velo (m .4 0. .2 0. .7 1.	ocity Flov /s) .930 .776 .077	v/Cap 0.177 0.278 0.903	Link /ol (m ³) 0.4178 0.2274 2.2718	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N 15 minute winter S1 15 minute winter S2 15 minute winter S3 15 minute winter S4	JS ode	Link 7.000_1 7.001_1 2.002 3.000	S2 SV S5 S3	DS Node V-A3 MH1	Outflor (I/s) 10. 70. 59.	w Velc (m .4 0. .2 0. .7 1. .7 2.	ocity Flow /s) .930 .776 .077 .411	v/Cap 0.177 0.278 0.903 0.647	Link vol (m ³) 0.4178 0.2274 2.2718 0.8453	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N 15 minute winter S1 15 minute winter S2 15 minute winter S2 15 minute winter S4 15 minute winter S4	JS ode	Link 7.000_1 7.001_1 2.002 3.000 2.003	S2 SV S5 S3 S6	DS Node V-A3 MH1	Outflor (I/s) 10. 70. 59. 85.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1.	ocity Flow /s) .930 .776 .077 .411 .291	v/Cap 0.177 0.278 0.903 0.647 1.085	Link /ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N (Upstream Depth) 15 minute winter 52 15 minute winter 52 15 minute winter 54 15 minute winter 54 15 minute winter 55 15 minute winter 55	JS ode	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003	S2 SV S5 S3 S6 S7	DS Node V-A3 MH1	Outflor (I/s) 10. 10. 70. 59. 85. 95.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1.	bcity Flow .930 .776 .077 .411 .291 .854	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908	Link /ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N (Upstream Depth) 15 minute winter 52 15 minute winter 53 15 minute winter 54 15 minute winter 55 15 minute winter 55 15 minute winter 56	JS ode	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004	S2 SV S5 S3 S6 S7 S1	DS Node V-A3 MH1	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2.	bcity Flow /s) .930 .776 .077 .411 .291 .854 .759	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533	Link 70l (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) 15 minute winter 52 15 minute winter 53 15 minute winter 53 15 minute winter 54 15 minute winter 55 15 minute winter 56 15 minute winter 57 15 minute winter 57	JS ode	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.003 5.004 1.006	S2 SV S5 S3 S6 S7 S1 S9	DS Node V-A3 MH1	Outflor (I/s) 10. 70. 59. 85. 95. 108. 191.	w Velc (m .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1.	bcity Flow /s) .930 .776 .077 .411 .291 .854 .759 .492	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632	Link 701 (m ³) 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N 15 minute winter S1 15 minute winter S2 15 minute winter S2	JS pode	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007	S2 SW S5 S3 S6 S7 S1 S9 SV	DS Node V-A3 MH1 1 V-2.2	Outflor (l/s) 10. 70. 59. 85. 95. 108. 191. 198.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .5 1.	beity Flow .930 .776 .077 .411 .291 .854 .759 .492 .552	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.422	Link /ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6085	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N 15 minute winter S2 15 minute winter S2	JS ode	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007	S2 SV S5 S3 S6 S7 S1 S9 SV SV	DS Node V-A3 MH1 1 V-2.2 V-2.2	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 20.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .5 1. .9 0.	Decity Flow .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .737	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.139	Link vol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 4.2070	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N 15 minute winter S2 15 minute winter S2 15 minute winter S3 15 minute winter S4 15 minute winter S5 15 minute winter S5 15 minute winter S5 15 minute winter S5 360 minute winter S1 360 minute winter S1	JS ode	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009	S2 SV S5 S3 S6 S7 S1 S9 SV SV S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .4 2. .5 1. .9 0. .2 0.	Decity Flow .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128	Link 70l (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878	Discharge Vol (m ³) 4.5
Link Event (Upstream Depth) N (Upstream Depth) 15 minute winter 52 15 minute winter 53 15 minute winter 54 15 minute winter 55 15 minute winter 55 15 minute winter 55 15 minute winter 55 15 minute winter 55 360 minute winter 51 360 minute winter 51	JS ode	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration	S2 SW S5 S3 S6 S7 S1 S9 SW SV SV S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .5 1. .9 0. .2 0.	Decity Flow .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .539	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128	Link 70l (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878	Discharge Vol (m ³) 4.5
Link EventN(Upstream Depth)N15 minute winterS115 minute winterS215 minute winterS2360 minute winterS1360 minute winterS1	JS ode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake	S2 SW S5 S3 S6 S7 S1 S9 SV SV S1 2* SV S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .4 2. .4 2. .5 1. .9 0. .2 0. .5	Decity Flow .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128	Link ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878	Discharge Vol (m³) 4.5
Link Event (Upstream Depth) 15 minute winter 52 15 minute winter 52 360 minute winter 51 360 minute winter 51 36	JS pode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake	S2 SW S5 S3 S6 S7 S1 S9 SV SV SV SV SV S8	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97.	w Velc (m .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .5 1. .9 0. .2 0. .5 .5	Decity Flow .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740	Link 701 (m ³) 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878	Discharge Vol (m³) 4.5
Link EventN(Upstream Depth)N15 minute winterS115 minute winterS215 minute winterS2360 minute winterS1360 minute winter	JS ode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake	S2 SW S5 S3 S6 S7 S1 S9 SV SV SV SV S1 	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5 4	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .5 1. .9 0. .2 0. .5 .5 1. .5 1. .5 1.	Decity Flow .930 .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161	Link vol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377	Discharge Vol (m³) 4.5
Link EventN(Upstream Depth)N15 minute winterS115 minute winterS215 minute winterS2360 minute winterS1360 minute winterS1360 minute winterS1360 minute winterS115 minute	JS ode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake 1.005 1.004 1.003	S2 SW S5 S3 S6 S7 S1 S9 SW S1 SW S1 SW S1 S1 S1 S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5 4 5	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91. 86.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .4 2. .5 1. .9 0. .2 0. .0 .5 . .1 2. .5 1. .4 1. .4 1. .2 1. .2 0. .2 0. .2 0. .2 0. .2 0. .2 0. .2 0. .2 0. .2 0. .2 1. .2 1. .4 1. .4 1. .4 1. .5 1. .2 0. .4 1. .4 1. .4 1. .4 1. .5 1. .2 0. .4 1. .4 1. .4 1. .5 1. .2 0. .4 1. .4 1. .4 1. .5 1. .2 0. .4 1. .4 1. .5 1. .2 0. .4 1. .2 0. .4 1. .2 0. .4 1. .2 0. .4 1. .5 1. .2 0. .4 1. .2 0. .4 1. .2 0. .4 1. .5 1. .2 0. .4 1. .2 0. .5 1. .2 0. .2 0. .2 0. .2 0. .2 0. .4 1. .5 1. .2 0. .2 0.0 .2 02 0.	Decity Flow .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001 .557 .236	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161 1.100	Link ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377 3.3334	Discharge Vol (m³) 4.5
Link EventN(Upstream Depth)N15 minute winterS215 minute winterS2360 minute winterS1360 minute winterS1360 minute winterS1360 minute winterS115 minute	JS ode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake 1.005 1.004 1.003 1.002	S2 SW S5 S3 S6 S7 S1 S9 SW S1 SW S1 S1 S1 S1 S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5 4 5 6	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91. 86. 78.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .4 2. .5 1. .9 0. .5 1. .5 1. .5 1. .4 1. .5 1. .9 0. .5 1. .9 0. .5 1. .9 0. .5 1. .9 0. .5 1. .1 2. .9 0. .5 1. .1 2. .9 0. .5 1. .1 2. .9 0. .5 1. .1 3. .2 0. .1 4. .2 1. .2 1. .2 1. .3 1. .4 1. .2 1. .3 1. .4 1. .5 1. .0 1. .0 1. .5 1. .0 1. .0 1. .5 1. .0 1. .5 1. .0 1. .5 1. .0 1. .0 1. .5 1.5 1. .5 1	Decity Flow .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001 .557 .236 .189	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161 1.100 1.005	Link ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377 3.3334 4.0923	Discharge Vol (m³) 4.5
Link EventN(Upstream Depth)N15 minute winterS215 minute winterS2360 minute winterS1360 minute winterS1360 minute winterS115 minute	JS pode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake 1.005 1.004 1.003 1.002 1.001	S2 SW S5 S3 S6 S7 S1 S9 SW S1 SW S1 S1 S1 S1 S1 S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5 4 5 6 7	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91. 86. 78. 42.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .5 1. .9 0. .2 0. .0 .5 . .1 2. .5 1. .9 1. .5 1. .9 1. .6 1.	Decity Flow .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001 .557 .236 .189 .070	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161 1.100 1.005 1.164	Link 701 (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377 3.3334 4.0923 1.0364	Discharge Vol (m³) 4.5
Link EventN(Upstream Depth)N15 minute winterS115 minute winterS215 minute winterS2360 minute winterS1360 minute winterS1360 minute winterS115 minute	JS ode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake 1.005 1.004 1.003 1.002 1.001 1.000	S2 SW S5 S3 S6 S7 S1 S9 SW S1 SW S1 S1 S1 S1 S1 S1 S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5 4 5 6 7 8	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91. 86. 78. 42. 41.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .4 2. .5 1. .9 0. .5 1. .9 0. .5 1. .9 1. .5 1. .4 1. .5 1. .9 1. .5 1. .4 1. .5 1.5 1. .5 1	Decity Flow .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001 .557 .236 .189 .070 .099	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161 1.100 1.005 1.164 0.981	Link ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377 3.3334 4.0923 1.0364 2.5668	Discharge Vol (m ³) 4.5
Link EventN(Upstream Depth)N15 minute winterS115 minute winterS215 minute winterS2360 minute winterS1360 minute winterS1360 minute winterS115 minute winterS1360 minute winterS1<	JS pode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake 1.005 1.004 1.003 1.002 1.001 1.000 6.006	S2 SW S5 S3 S6 S7 S1 S9 SV SW S1 S1 S1 S1 S1 S1 S1 S1	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5 4 5 6 7 8 0	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91. 86. 78. 42. 41.	w Velc (m .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .2 1. .5 1. .9 0. .2 0. .5 . .1 2. .5 1. .9 1. .5 1. .4 1. .5 1. .9 1. .5 1. .2 0. .5 1. .2 0. .5 1. .2 0. .5 1. .2 0. .2 0. .5 1. .2 0. .2 0.0 .2	Decity Flow .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001 .557 .236 .070 .099 .696 .696	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161 1.100 1.005 1.164 0.981 0.143	Link ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377 3.3334 4.0923 1.0364 2.5668 0.6857	Discharge Vol (m ³) 4.5
Link EventN(Upstream Depth)N15 minute winterS115 minute winterS215 minute winterS2360 minute winterS1360 minute winterS115 minute winterS1360 minute winterS115 minute winterS1360 minute winterS2360 minute winterS2360 minute winterS2360 minute winterS2360 minute winterS2360 minute winterS2<	JS ode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake 1.005 1.004 1.003 1.002 1.001 1.000 6.006 6.005	S2 SW S5 S3 S6 S7 S1 S9 SW S1 S1 S1 S1 S1 S1 S1 S1 S1 S2	DS Node V-A3 MH1 1 V-2.2 V-2.2 2 V- A3 MH5 4 5 6 7 8 0 0	Outflor (I/s) 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91. 86. 78. 42. 41.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .4 2. .5 1. .9 0. .5 1. .9 0. .5 1. .9 0. .5 1. .4 1. .5 1. .9 1. .5 1. .4 1. .5 1. .4 1. .5 1. .5 1. .5 1. .7 2. .0 . .7 2. .0 . .7 2. .0 . .7 2. .0 . .2 0. .0 0. .5 1. .2 0. .2 0. .5 1. .2 0. .5 1. .5 1.5 1. .5	Decity Flow .930 .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001 .557 .236 .189 .070 .099 .696 .728 .728	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161 1.100 1.005 1.164 0.981 0.143 0.143 0.148	Link ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377 3.3334 4.0923 1.0364 2.5668 0.6857 1.1483	Discharge Vol (m ³) 4.5
Link EventN(Upstream Depth)N15 minute winterS115 minute winterS215 minute winterS2360 minute winterS1360 minute winterS1360 minute winterS115 minute winterS1360 minute winterS1360 minute winterS1360 minute winterS1360 minute winterS1360 minute winterS1360 minute winterS2360 minute winterS2	JS ode 	Link 7.000_1 7.001_1 2.002 3.000 2.003 5.003 5.004 1.006 1.007 4.007 1.009 Infiltration Hydro-Brake 1.005 1.004 1.003 1.002 1.001 1.000 6.006 6.005 6.004	S2 SW S5 S3 S6 S7 S1 S9 SW S1 S1 S1 S1 S1 S1 S1 S1 S1 S2 S2	DS Node V-A3 MH1 1 V-2.2 V-2.2 V-A3 MH5 4 5 6 7 8 0 0 1	Outflor (I/s) 10. 10. 10. 70. 59. 85. 95. 108. 191. 198. 10. 39. 0. 16. 97. 91. 86. 78. 42. 41. 11. 13.	w Velc (m .4 0. .2 0. .7 1. .7 2. .0 1. .4 1. .4 2. .5 1. .9 0. .2 0. .5 1. .9 0. .5 1. .9 1. .6 1. .5 1. .9 1. .6 1. .7 0. .6 0.	Decity Flow .930 .930 .776 .077 .411 .291 .854 .759 .492 .552 .737 .539 .001 .557 .236 .189 .070 .099 .696 .728 .991 .991	v/Cap 0.177 0.278 0.903 0.647 1.085 0.908 0.533 0.632 0.870 0.139 0.128 0.740 1.161 1.100 1.005 1.164 0.981 0.143 0.143 0.148 1.054	Link ol (m ³) 0.4178 0.2274 2.2718 0.8453 2.1534 1.9386 0.7155 2.6162 2.6085 0.6783 1.2878 2.4233 0.4377 3.3334 4.0923 1.0364 2.5668 0.6857 1.1483 1.3410	Discharge Vol (m³) 4.5



Page 10 20-074 Church Fields Church Field East Surface water - 5 Years

Results for 5 year +20% CC Critical Storm Duration. Lowest mass balance: 99.71%

US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
S24	11	81.811	0.183	26.1	0.3274	0.0000	ОК
S25	12	81.822	0.123	18.7	0.1530	0.0000	ОК
S26	10	81.848	0.096	11.8	0.1910	0.0000	ОК
S27	11	83.043	0.483	53.1	1.4345	0.0000	SURCHARGED
S28	11	83.073	0.436	25.7	1.3527	0.0000	SURCHARGED
S29	10	82.375	0.044	5.5	0.0656	0.0000	ОК
S30	1	81.970	0.000	0.0	0.0000	0.0000	ОК
S31	10	82.532	0.315	94.1	0.9467	0.0000	SURCHARGED
1	11	83.215	0.065	1.3	0.0731	0.0000	ОК
SW-2.1	1	83.245	0.000	0.0	0.0000	0.0000	ОК
SW-2.2	280	81.647	0.723	51.8	1.2767	0.0000	SURCHARGED
SW-2.3	280	81.646	0.780	51.2	1.3787	0.0000	SURCHARGED
	US Node S24 S25 S26 S27 S28 S29 S30 S31 1 SW-2.1 SW-2.1 SW-2.2 SW-2.3	USPeakNode(mins)S2411S2512S2610S2711S2811S2910S301S31100111SW-2.1280SW-2.3280	USPeakLevelNode(mins)(m)S241181.811S251281.822S261081.848S271183.043S281183.043S291082.375S30181.970S311082.53211183.245SW-2.1183.245SW-2.228081.647SW-2.328081.646	USPeakLevelDepthNode(mins)(m)(m)S241181.8110.183S251281.8220.123S261081.8480.096S271183.0430.483S281183.0730.436S291082.3750.044S30181.9700.000S311082.5320.31511183.2150.065SW-2.1183.2450.000SW-2.228081.6470.723SW-2.328081.6460.780	USPeakLevelDepthInflowNode(mins)(m)(l/s)S241181.8110.18326.1S251281.8220.12318.7S261081.8480.09611.8S271183.0430.48353.1S281183.0730.43625.7S291082.3750.0445.5S30181.9700.0000.0S311082.5320.31594.111183.2450.0051.3SW-2.1183.2450.0000.0SW-2.228081.6470.72351.8SW-2.328081.6460.78051.2	USPeakLevelDepthInflowNodeNode(mins)(m)(m)(l/s)Vol (m³)S241181.8110.18326.10.3274S251281.8220.12318.70.1530S261081.8480.09611.80.1910S271183.0430.48353.11.4345S281183.0730.43625.71.3527S291082.3750.0445.50.0656S30181.9700.0000.00.0000S311082.5320.31594.10.946711183.2150.0651.30.0731SW-2.1183.2450.0000.00.0000SW-2.228081.6470.72351.81.2767SW-2.328081.6460.78051.21.3787	USPeakLevelDepthInflowNodeFloodNode(mins)(m)(m)(l/s)Vol (m3)(m3)S241181.8110.18326.10.32740.0000S251281.8220.12318.70.15300.0000S261081.8480.09611.80.19100.0000S271183.0430.48353.11.43450.0000S281183.0730.43625.71.35270.0000S291082.3750.0445.50.06560.0000S30181.9700.0000.00.00000.0000S311082.5320.31594.10.94670.000011183.2450.0000.00.00000.0000SW-2.1183.6470.72351.81.27670.0000SW-2.328081.6460.78051.21.37870.0000

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (I/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
15 minute winter	S24	6.002	S23	23.9	0.734	0.655	1.1407	
15 minute winter	S25	6.001	S24	17.9	0.762	0.489	0.4021	
15 minute winter	S26	7.001	S25	11.6	0.625	0.318	0.2024	
15 minute winter	S27	5.001	S31	51.0	1.283	1.320	1.9178	
15 minute winter	S28	5.000	S27	22.9	0.660	0.539	0.4568	
15 minute winter	S29	4.000	S25	5.5	0.482	0.085	0.5679	
15 minute summer	S30	7.000	S26	0.0	0.000	0.000	0.2263	
15 minute winter	S31	5.002	S8	93.1	1.372	1.130	0.6600	
15 minute winter	1	7.000_2	S3	-1.3	-0.092	-0.026	0.3909	
15 minute summer	SW-2.1	3.000_1	S8	0.0	0.000	0.000	0.0000	
360 minute winter	SW-2.2	1.008	SW-2.3	51.2	0.772	0.224	1.8288	
360 minute winter	SW-2.3	1.009_1	S11	50.7	1.172	0.221	0.9755	

Appendix F

Attenuation Design – 1, 30 & 100 Year Storms (+20% Climate change)

42 Engineering Assessment Report Project Number: 20-074 Document Reference: 20-074r.4001

	Waterman	Moylan	Consultir	ng File	: 4A new R1	1.pfd		Page 1		
CAUSEWAY 🛟				Net	work: Storr	n Network		20-074 (Church Field	ls
					iarth Kurell	а		Attonuo	Fields East	Storm
				25/	04/2025			Allenua	LIONITIEALS	storm
			Desi	ign Settiı	<u>ngs</u>					
Rainfall Methodolo	egy ESR			Maxim	um Time of	Concentrati	ion (m	ins) 30	.00	
Beturn Period (vea	rs) 5			i i i axii i i	Maxir	num Rainfal	l (mm	/hr) 50	0	
Additional Flow (%) 0				Mi	inimum Velo	citv (n	n/s) 0.7	75	
FSR Regi	on Scotlan	d and Ire	eland			Connec	tion T	vpe Le	vel Soffits	
M5-60 (m	m) 16.800				Minimum	n Backdrop H	leight	(m) 0.6	500	
Ratic	p-R 0.270				Prefe	erred Cover I	Depth	(m) 1.5	200	
	CV 0.750				Include	Intermediat	e Grou	und √		
Time of Entry (mi	ns) 4.00			E	Inforce best	t practice de	sign ru	ules √		
				Nodes						
	N	•	T . (F	Course	F actions		Dent			
	Name	Area (ha)	(mins)	Level	Easting (m)	(m)	Dept (m)	n		
De	onth/Aroa 1	1 960	4 00	(m) 82 900	13 556	61 037	2.06	5		
		1.500	4.00	02.900	13.550	01.057	2.00	5		
			<u>Simula</u>	ation Set	<u>tings</u>					
Rainfall M	ethodology	FSR				Analysis S	peed	Detailed	d	
	FSR Region	Scotlar	nd and Ire	land	9	Skip Steady S	State	х		
N	15-60 (mm)	16.800			Drain D	own Time (r	nins)	240		
	Ratio-R	0.270			Additiona	l Storage (m	³/ha)	20.0		
9	Summer CV	0.750			Check [Discharge Ra	te(s)	х		
	Winter CV	0.840			Check D	ischarge Vol	ume	х		
			Stor	n Durati	one					
15 60	180	360	600	960	2160	4320	7200	100	080	
30 120	240	480	720	1440	2880	5760	8640			
R	eturn Period	Clima	te Chang	e Addi	tional Area	Addition	al Flov	v		
	(vears)	() ()	CC %)		(A %)	(0 %	ai i iov %)			
	1		2	0	0)	-, (C		
	Nod	<u>e Depth</u>	/Area 1 (Online Hy	<u>/dro-Brake®</u>	[®] Control				
F	lap Valve 🛛 🗙				Objective	e (HE) Min	imise u	upstream	n storage	
Replaces Downstr	eam Link 🗸	/		Sur	np Available	e√				
Invert	Level (m) 8	0.800		Produ	uct Number	CTL-SHE-	0162-1	1680-250	0-1680	
Design D	epth (m) 2	.500	Min	Outlet Di	ameter (m)	0.225				
Design	Flow (l/s) 1	.6.8	Min N	lode Diar	neter (mm)	1800				
	Node	e Depth,	/Area 1 D	epth/Ar	ea Storage	<u>Structure</u>				
Base Inf Coefficien	t (m/hr) 0.	06300	Safety	v Factor	1.0	Ir	ivert L	evel (m)	80.835	
Side Inf Coefficien	t (m/hr) 0.	06300	F	Porosity	0.40	Time to half	empt	y (mins)	0	
Denth <i>L</i>	Area Inf∆	rea	Denth	Area	Inf Area	Denth	Area	Inf ∆re	a	
(m) ((m^2) (m^2)	2)	(m)	(m ²)	(m ²)	(m)	(m ²)	(m ²)	-	
0 000 11	, (iii	0.0	1.765	1170 0	0.0	1 766	0.0	1100	0	
0.000 1			1.705		0.0	1.700	0.0	1100.	-	



Results for 1 year +20% CC Critical Storm Duration. Lowest mass balance: 99.49%

Node Event	US Node	Pea (mir	ık Leve ıs) (m)	l Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
360 minute win	ter Depth/Ar	ea 1 2	64 81.35	0 0.515	53.7	250.8400	0.0000	ОК
	Link Event	U	IS	Link	Outfl	ow Disc	narge	
(L	pstream Dept	h) No	ode		(I/s	s) Vol	(m³)	
36	60 minute wint	er Depth,	/Area 1 H	lydro-Brak	e® 1	6.3	428.3	
36	50 minute winte	er Depth,	/Area 1 I	nfiltration		0.0		

	Waterman	Moylan	Consultir	ng File	e: 4A new Rí twork: Storr	1.pfd m Network		Page 1 20-074 Church Fields	
CAUSEWAT 🚺				Sid	harth Kurell	a		Church Fields East	
				25/	/04/2023			Attenuation 30 Years Sto	orm
			<u>Desi</u>	ign Setti	ngs				
Rainfall Methodolog	gy FSR			Maxim	um Time of	Concentrati	on (mi	ins) 30.00	
Return Period (year	s) 5				Maxir	num Rainfal	l (mm/	′hr) 50.0	
۸dditional Flow (۹	6) 0				Mi	inimum Velo	city (n	n/s) 0.75	
FSR Regio	n Scotlan	d and Ir	eland			Connec	tion T	pe Level Soffits	
M5-60 (mn	n) 16.800				Minimum	n Backdrop H	leight	(m) 0.600	
Ratio-	R 0.270				Prefe	erred Cover L	Depth	(m) 1.200	
Time of Entry (min	V 0.750				Include Enforce bos	Intermediat t practico do	e Grol	ina √	
Time of Entry (min	5) 4.00				Emorce bes	t practice de	sign ru	nes v	
				<u>Nodes</u>					
	Name	Area (ha)	T of E (mins)	Cover Level	Easting (m)	Northing (m)	Dept (m)	h	
Dep	oth/Area 1	1.960	4.00	82.900	13.556	61.037	2.06	5	
			<u>Simula</u>	ation Set	<u>ttings</u>				
Rainfall Me	thodology	FSR				Analysis Sp	beed	Detailed	
F	SR Region	Scotlar	nd and Ire	land		Skip Steady S	state	х	
M	5-60 (mm)	16.800)		Drain D	own Time (n	nins)	240	
-	Ratio-R	0.270			Additiona	l Storage (m	∛ha)	20.0	
Si	ummer CV	0.750			Check I	Discharge Ra	te(s)	Х	
	Winter CV	0.840			Check D	ischarge Vol	ume	x	
15	100		Stori	n Durati	ions	4000		10000	
15 60 30 120	240	360 480	600 720	960 1440	2160	4320 5760	7200 8640	10080	
Re	turn Period	Clima	ite Chang	e Add	itional Area	Addition	al Flow	I	
	(years) 30		2	0	(~ /•)) (Q /	•) ()	
	Nod	o Donth	- /Area 1 () Nine H	vdro-Brake	® Control		-	
	1104				yuro bruke	<u></u>			
Fla	ap Valve x			C	Objective	e (HE) Mini	mise ι	ipstream storage	
Replaces Downstre	am Link v	/ 20 200		Sun	np Available	? √ 	0162 1	690 2500 1690	
Design De	ever(III) = a	500	Min	Piou Outlat D	iameter (m		0102-1	1060-2500-1060	
Design F	low (l/s) 1	.6.8	Min N	lode Dia	meter (mm)) 1800			
	Node	e Depth,	/Area 1 D	epth/Ar	ea Storage	<u>Structure</u>			
Base Inf Coefficient	(m/hr) 0.	06300	Safet	y Factor	1.0	In	vert Le	evel (m) 80.835	
Side Inf Coefficient	(m/hr) 0.	06300	F	Porosity	0.40	Time to half	empty	y (mins)	
Depth A	rea Inf A	rea	Depth	Area	Inf Area	Depth	Area	Inf Area	
(m) (r	n²) (m²	²)	(m)	(m²)	(m²)	(m)	(m²)	(m²)	
0.000 11	70.0	0.0	1.765	1170.0	0.0	1.766	0.0	1100.0	



Results for 30 year +20% CC Critical Storm Duration. Lowest mass balance: 99.14%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	N Va	lode ol (m³)	Flood (m³)	Status
480 minute winter	Depth/Area 1	456	82.199	1.364	88.1	664	4.4689	0.0000	ОК
Li	ink Event	US		Link	Outfl	ow	Discha	arge	
(Upst	ream Depth)	Node			(I/s	;)	Vol (r	n³)	
480 n	ninute winter	Depth/Are	a1 Hy	dro-Brake	® 1	6.5	57	70.0	
480 n	ninute winter	Depth/Are	a 1 Infi	iltration		0.0			

	Waterman	Moylan	Consultir	ng File	e: 4A new R1	L.pfd		Page 1	
				Net	twork: Storr	n Network		20-074 Church Fields	
CAUSEVVAI				Sid	harth Kurell	а		Church Fields East	
				25/	/04/2023			Attenuation 100 Years Stor	n
			Des	<u>ign Setti</u>	ngs				
Rainfall Methodolog	gy FSR			Maxim	um Time of	Concentratio	on (mi	ns) 30.00	
Return Period (year	s) 5				Maxir	num Rainfall	(mm/	hr) 50.0	
Additional Flow (9	%) 0				Mi	nimum Veloo	city (m	/s) 0.75	
FSR Regio	on Scotland	d and Ir	eland			Connect	tion Ty	pe Level Soffits	
M5-60 (mr	n) 16.800				Minimum	Backdrop H	eight (m) 0.200	
Ratio	, -R 0.270				Prefe	erred Cover D	epth (m) 1.200	
(V 0750				Include	Intermediate	- Grou		
Time of Entry (min	s) 4.00				Enforce hest	nractice des	ign ru		
Time of Endy (finit	3) 4.00			'			JEI I U		
				<u>Nodes</u>					
	Name	Area	T of E	Cover	Easting	Northing	Dept	n	
		(ha)	(mins)	Level (m)	(m)	(m)	(m)		
De	pth/Area 1	1.960	4.00	82.900	13.556	61.037	2.06	5	
			<u>Simul</u>	ation Set	<u>ttings</u>				
Rainfall Me	thodology	FSR				Analysis Sp	eed	Detailed	
I	SR Region	Scotla	nd and Ire	eland	9	Skip Steady S	tate	x	
Μ	5-60 (mm)	16.800)		Drain D	own Time (m	ins)	240	
	Ratio-R	0.270			Additiona	l Storage (m ³	/ha)	20.0	
S	ummer CV	0.750			Check [Discharge Rat	e(s)	x	
	Winter CV	0.840			Check D	ischarge Volu	ume	х	
			C 1			-			
15 60	190	260	Stor		2160	1220	7200	10090	
20 120	240	190	720	900	2100	4320	7200 9640	10080	
30 120	240	400	720	1440	2000	5700	8040		
Re	turn Period	Clima	ate Chang	e Add	itional Area	Additiona	I Flow	,	
	(vears)		(CC %)	,	(A %)	(Q %	5)		
	100		2	0	0)	, ()	
			_	-	-				
	Node	e Depth	n/Area 1 (Online H	ydro-Brake [®]	[®] Control			
FI	ap Valve x				Obiective	e (HE) Minii	mise u	pstream storage	
Replaces Downstre	am Link 🗸	/		Sun	np Available	(··_, ·····			
Invert I	evel (m) 8	0 800		Prod	uct Number	· · · · · · · · · · · · · · · · · · ·)162-1	680-2500-1680	
Design D	e^{1} (m) 2	500	Min	Outlet D	iameter (m)	0.225			
Design F	low(l/s) = 1	68	Min N	lode Dia	meter (mm)	1800			
Designi	1011 (1/3)	0.0		oue blu		1000			
	Node	e Depth	/Area 1 D	epth/Ar	ea Storage	<u>Structure</u>			
Base Inf Coefficient	(m/hr) 0	06300	Safet	v Factor	10	Inv	vert le	evel (m) 80 835	
Side Inf Coefficient	: (m/hr) 0.0	06300		Porosity	0.40	Time to half	empty	/ (mins)	
Donth A	rea Inf A.	·	Donth	Area	Inf Area	Donth	Area	Inf Area	
	nea IIIIAI m²) /m²	ca	(m)	(m ²)	(m ²)	/m	Aied (m ²)	(m ²)	
(m) (i 0.000 11	יי ו ו (m™ 700 י		1 765	1170.0	(III) 0 0	1 766	0.0	())) 1100 0	
0.000 11	, 0.0	0.0	1.705	11/0.0	0.0	1.700	0.0	1100.0	



Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.13%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	N Vol	ode (m³)	Flood (m³)	Status
480 minute winter	Depth/Area 1	352	82.610	1.775	110.8	860	.1888	0.0000	ОК
 (11ac	.ink Event	US Nodo		Link	Outfl	ow	Discha	nrge	
(Ups 480	minute winter	Depth/Are	a1 Hvo	dro-Brake	(1/S ® 1	6.5	voi (i 55	58.1	
480	minute winter	Depth/Are	a1 Infi	Itration	-	9.3			

Appendix G

Attenuation Capacity Checks (Catchments A3 & A4)

43 Engineering Assessment Report Project Number: 20-074 Document Reference: 20-074r.4001

111	waterman
	mogium

Church Fields A3 & Church Field East	
Catchment	
Roofs(m²)	3961.899
Roads (m²)	6180.095
Permeable paving (m ²)	1790.415
Grass (m²)	11650.046
Total Drained Area of New Development (m ²)	<u>23582.455</u>
Paved Area Factors (PIMP Factors)	
Roofs(m²)	0.95
Roads (m²)	0.95
Permeable paving (m ²)	0.95
Grass (m²)	0.05
Paved Area Factors (m ²)	
Roofs(m²)	3763.80405
Roads (m ²)	5871.09025
Permeable paving (m ²)	1700.89425
Grass (m²)	582.5023
PIMP factor for Site 4	
Element	
Roofs	16.0%
Roads	24.9%
Permeable paving	7.2%
Grass	2.5%
Impermeable Area ha	<u>50.5388%</u> <u>1.19183</u> ha
Greenfield Outflow	
Total Allowed based on 3.7litres/second/hectare	
Site Area (Ha)	2.36
QBar formula	3.7x (Site area Ha)
Qbar allowed ouflow for Total Area (I/s)	8.73 (+ 16.8 Sector 4) 25.50 l/s

M:\Projects\20\20-074 - Churchfields\Design\Civil\02 Sector 4\01 Surface water\Flow\Sector 3 check\A3\2023-04-14 - Paved Area Factors.xlsx

AUSEWAY 🛟	Waterman Moylan Consul	ting File: 202 Networl Sidharth 25/04/2	3-04-14 - a3.pfd :: Storm Network Kurella 023	Page 1 20-074 Church F Catchme	Fields Housing and Eas ent A3
	<u>D</u>	<u>esign Settings</u>			
Rainfall Methodolo Return Period (yea Additional Flow FSR Reg M5-60 (m Ratio	Dgy FSR ars) 5 (%) 0 ion Scotland and Ireland im) 16.800 o-R 0.270 CV 0.750 ins) 4.00	Maximum T Mi I Enfor	ime of Concentratio Maximum Rainfall (Minimum Veloci Connecti nimum Backdrop He Preferred Cover De nclude Intermediate ce best practice desi	n (mins) 30 mm/hr) 50 ty (m/s) 1.0 on Type Lev ight (m) 0.2 epth (m) 1.2 Ground \checkmark gn rules \checkmark	.00 .0 00 vel Soffits 200 200
		<u>Nodes</u>			
Name	Area T of E Add (ha) (mins) Inflow (l/s)	Cover Dia Level (r (m)	meter Easting N nm) (m)	orthing De (m) (r	pth n)
Depth/Area 1	1 1.192 4.00 16.8	78.650 78.980	3.021 1200 4.619	60.2012.459.1811.4	453 500
		<u>Links</u>			
NameUSDSNodeNode1.0001	6 Length ks (mm) / de (m) n Area 1 1.896 0.600	US IL DS (m) (r 77.480 76.	IL Fall Slope n) (m) (1:X) 197 1.283 1.5	Dia T (mm) (m 100	of C Rain hins) (mm/hr) 4.00 50.0
Name 1.000	Vel Cap Flow US (m/s) (l/s) (l/s) Dept (m) 6.415 50.4 16.8 1.40	DS Σ/ h Depth (l (m) 0 2.353 0	Area ΣAdd Pro na) Inflow Dep (I/s) (mn 000 16.8 Ξ	o Pro th Velocity n) (m/s) 39 5.755	
	<u>Pip</u>	eline Schedule			
Link Length S (m) 1.000 1.896 Lir 1.0	Slope Dia Link U (1:X) (mm) Type 1.5 100 Circular 78 nk US Dia Node Node (mm) Type 00 1 1200 Manho	JS CL US IL (m) (m) 8.980 77.480 e MH e Type ple Adoptable	US Depth DS Cl (m) (m) 1.400 78.650 DS Node Depth/Area 1 Ju	DS IL (m) 0 76.197 Node Type unction	DS Depth (m) 2.353
	Ma	nhole Schedule			
Node East (n	ting Northing CL n) (m) (m)	Depth Dia (m) (mm)	Connections	Link IL (m	Dia) (mm)
Depth/Area 1 3.	021 60.201 78.650	2.453	1	1.000 76.1	97 100
1 4.	619 59.181 78.980	1.500 1200	° ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	1 000 77 4	

CAUSEWAY 🛟	Waterman Moylan Consu	ulting File Ne Sid	e: 2023-04-14 twork: Storm harth Kurella	- a3.pfd Network	Page 2 20-074 Church Fields Housing and East
	l Sin	nulation Set	04/2023		
Rainfall M	lethodology FSR FSR Region Scotland and A5-60 (mm) 16.800 Ratio-R 0.270 Summer CV 0.750 Winter CV 0.840	d Ireland	Sk Drain Do Additional S Check Di Check Dis	Analysis Speed ip Steady State wn Time (mins Storage (m ³ /ha scharge Rate(s	d Normal e x) 240) 20.0) x
	S	torm Durati	ions	charge volume	~ ^
15 60 30 120	180 360 600 240 480 720	960 1440	2160 2880	4320 720 5760 864	00 10080 40
R	eturn Period Climate Cha (years) (CC %) 100	ange Add	itional Area (A %) 0	Additional Flo (Q %)	o w
	Node Depth/Area	1 Online H	ydro-Brake [®] (<u>Control</u>	
F Replaces Downstr Invert Design D Design	lap Valve x eam Link √ Level (m) 76.197 Depth (m) 1.500 M Flow (I/s) 25.5 Mi	Sur Prod 1in Outlet D in Node Dia	Objective np Available uct Number iameter (m) meter (mm)	(HE) Minimise ✓ CTL-SHE-0214 0.300 1800	e upstream storage 4-2550-1500-2550
	Node Depth/Area	1 Depth/Ar	<u>ea Storage St</u>	<u>ructure</u>	
Base Inf Coefficier Side Inf Coefficier	t (m/hr) 0.00000 Sa t (m/hr) 0.00000	ifety Factor Porosity	1.0 0.40 Ti	Invert me to half em	Level (m) 76.197 pty (mins)
Depth // (m) (0.000 12	Area Inf Area Dept (m ²) (m ²) (m) 200.0 0.0 1.45	h Area (m²) 0 1200.0	Inf Area (m²) 0.0	Depth Are. (m) (m ² 1.451 0.0	a Inf Area (m²) 0 0.0



720 minute winter 1

720 minute winter Depth/Area 1 Hydro-Brake®

1.000

25.5

16.8

6.145

0.334

0.0148

1269.1

Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.99%

Node Even	t	US Node	Peak (mins)	Level (m)	Depth (m)	n Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status	
720 minute wi	nter	Depth/Area 1	690	77.560	1.363	67.3	667.4916	0.0000	ОК	
720 minute wi	nter	1	690	77.777	0.297	16.8	0.3362	0.0000	SURCHAR	GED
Link Event (Upstream Depth)	U: No	S de	Link	DS Node	9	Outflow (I/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)

Depth/Area 1



User Inputs

SC-740

Chamber Model:

<u>Results</u>

System Volume and Bed Size

Outlet Control Structure:	Yes	Installed Storage Volume:	638.26 cubic meters.
Project Name:	Church Fields A3	Storage Volume Per Chamber:	1.30 cubic meters.
Engineer:	Noel Mahon	Number Of Chambers Required:	234
Project Location:		Number Of End Cans Required:	24
Measurement Type:	Metric	Chamber Deurs	17
Required Storage Volume:	623.01 cubic meters.		17
Stone Porosity:	40%	Maximum Length:	32.84 m.
Stone Foundation Depth:	351 mm.	Maximum Width:	25.26 m.
Stone Above Chambers:	300 mm.	Approx. Bed Size Required:	806.97 square me- ters.
Average Cover Over Chambers:	458 mm.	System Compor	nents
Design Constraint Dimensions:	(26.00 m. x 33.01 m.)	Amount Of Stone Required:	836 cubic meters
		Volume Of Excavation (Not Including Fill):	3 1140 cubic meters
		Total Non-woven Geotextile Require	d: 2138 square meters
		Woven Geotextile Required (excludir Isolator Row):	1g 67 square meters
		Woven Geotextile Required (Isolator Row):	57 square meters
		Total Woven Geotextile Required:	123 square meters
		Impervious Liner Required:	0 square meters
EMBEDMENT STONE SHALL BE A CLEAN, CRUSHED AND ANGULAR STONE WITH AN AASHTO M43 DESIGNATION BETWEEN #3 AND #57 CHAMBERS SHALL MEET THE REQUIREMENTS FOR ASTM F2418 POLYPROPLENE (PP) CHAMBERS OR ASTM F922 POLYETHYLENE (PE) CHAMBERS ADS GEOSYTHETICS 601T NON-WOVEN GEOTEXTILE ALL AROUND CLEAN, CRUSHED, ANGULAR EMBEDMENT STONE		GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES FINES, COMPACT IN 6° (150 mm) MAX LIFTS TO 95% PROC DENSITY. SEE THE TABLE OF ACCEPTABLE FILL MATERIA CHAMBERS SHALL BE BE DESIGNED IN ACCORDANCE W "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF TH CORRUGATED WALL STORMWATER COLLECTION CHAME PAVEMENT LAYER (DESIGNED BY SITE DESIGN ENGINEER)	<35% ITOR LS. ITH ASTM F2787 ERMOPLASTIC JERS".
ちちょうちょう ないりょう しょうしょう しょうしょう	いちょうちょう ひんりょう ひょうしょう	こうちゅうり はんしん ひんしん ひんしんしん	. 8' 18" (2.4 m)



MINIMUM COVER TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 24 (600 mm).

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W	moylan

Project :	Church Fields A4 & Church Field East
WM Ref:	20-074
Title:	Paved Area Factors
Date:	Apr-23

Element Linear park (m ²)	10841.23	
Catchment		
Roots, Roads and Permiable paving (m ²)	8876.825	
Total Drained Area of New Development (m ²)	5405.438 14282.263	
Total Drained Area of New Development including linear park (m²)	<u>25123.493</u>	
Paved Area Factors (PIMP Factors)		
Roofs, Roads and Permiable paving	0.95	
Grass	0.05	
Davied Area Factors (m ²)		
Paved Area Factors (m ⁻)		
Roofs, Roads and Permiable paving (m ²)	8432.98	
Grass (m²)	270.27	
Linear park (m²)	4040	
PIMP factor for Site 4		
Element		
Roofs, Roads and Permiable paving	33.6%	
Grass	1.1%	
Linear park	16.1%	
Average PIMP Factor Per site	<u>50.722%</u>	
Impermeable Area na	<u>1.27433</u> na	
Greenfield Outflow		
Total Allowed based on 3.7litres/second/hectare		
Site Area (Ha)	2.51	
QBar formula	3.7x(Site area Ha)	

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	Waterman Moyl	an Consulting	File: A4.pf	d		Page 1	
			Network:	Storm Netw	ork	20-074	
			Sidharth K	urella		Church Fi	elds Housing and East
			25/04/202	23		Catchmer	nt A4
		<u>Design</u>	<u>Settings</u>				
Rainfall Methodolo	gy FSR	M	aximum Tin	ne of Conce	ntration (n	nins) 30.0	00
Return Period (yea	rs) 5		Ν	/laximum Ra	ainfall (mn	n/hr) 50.0)
Additional Flow (%) 0			Minimum	Velocity (m/s) 1.00	C
FSR Regi	on Scotland and	l Ireland		Co	onnection	Type Lev	el Soffits
M5-60 (m	m) 16.800		Mini	mum Backd	rop Heigh	t (m) 0.60	00
Ratio	o-R 0.270			Preferred Co	over Depth	n (m) 1.20	00
	CV 0.750		Inc	lude Interm	ediate Gro	ound √	
Time of Entry (mi	ns) 4.00		Enforce	best practi	ce design i	rules √	
	,	I		•	0		
		No	des				
	Name	Area Cover	Easting	Northing	Depth		
		(ha) Level	(m)	(m)	(m)		
		(m)					
	Depth/Area 1	1.273 76.000	3.021	60.201	2.115		
		Simulatio	<u>n Settings</u>				
Painfall M	athodology FSP			٨٥٩	usic Spood	Normal	
Rainian M	ECD Decier Con	المعامية المعامية	4	Alidi Chin Ch	ysis speed	Normai	
	FSR Region SCO	tiand and Ireian	a Dr	SKIP Sti SKIP Sti	eady State	X 240	
IN IN		500	Ur Andri		me (mms)	240	
		70	Addi	tional Stora	ge (m7na)	20.0	
	Summer CV 0.7:	50		ieck Dischai	ge Rate(s)	X	
	winter CV 0.84	40	Ch	eck Dischar	ge volume	х	
		Storm D	urations				
15 60	180 360	600 0		60 432	0 720	0 1009	20
30 120	2/0 /80	720 1	1/0 28	80 576	0 720	0 1000	30
50 120	240 400	720 1	200	50 570	0 004	0	
R	eturn Period Cli	mate Change	Additional	Area Add	itional Flo	w	
	(vears)	(CC %)	(A %)		(0 %)		
	100	20		0		0	
				-		-	
	Node De	oth/Area 1 Onli	ne Hydro-B	rake [®] Contr	<u>ol</u>		
F	lap Valve x		Obje	ctive (HE)	Minimise	upstream	storage
Replaces Downstr	eam Link √		Sump Avai	lable √			
Invert	Level (m) 73.885	5	Product Nu	mber CTL	-SHE-0131	-9300-1690)-9300
Design D	epth (m) 1.690	Min Out	let Diamete	r (m) 0.15	50		
Design	Flow (l/s) 9.3	Min Node	e Diameter (mm) 120	0		
	Node Dou	4h /A 4 Double	L /A				
	Node Dep	th/Area 1 Dept	h/Area Stoi	rage Structu	<u>ire</u>		
Base Inf Coefficien	t (m/hr) 0.0000	0 Safety Fa	ctor 1.0		Invert	level (m)	73.885
Side Inf Coefficien	t (m/hr) 0.0000	0 Porc	sity 0.40	Time t	o half emp	tv (mins)	
	,, 0.0000		, 0.40		n	- ,	
Depth	Area Inf Area	Depth Are	ea Inf Are	a Dep	th Area	Inf Area	
(m)	(m²) (m²)	(m) (m	²) (m²)	(m	(m ²)	(m²)	
0.000	28.0 0.0	1.690 928	, ,, 3.0 0	.0 1.69	0.0	0.0	
			. 0		2.5	0.0	



Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.99%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
600 minute winte	Depth/Area 1	570	75.507	1.622	61.1	621.4820	0.0000	ОК
	Link Event	US		Link	Outfl	ow Discha	arge	
(Ups	tream Depth)	Node			(I/s) Vol (ı	m³)	
600	minute winter	Depth/Area	a1 Hy	dro-Brake	®	9.3 3	86.4	



User Inputs

MC-3500

Chamber Model:

<u>Results</u>

System Volume and Bed Size

Outlet Control Structure:	Yes	Installed Starses Volumes	CAO 70 subis motors
Project Name:	Church Fields A4	installed storage volume.	640.79 Cubic meters.
Engineer:	Noel Mahon	Storage Volume Per Chamber:	3.12 cubic meters.
Project Location:		Number Of Chambers Required:	117
Measurement Type:	Metric	Number Of End Caps Required:	22
Required Storage Volume:	621.01 cubic meters.	Chamber Rows:	11
Stone Porosity:	40%	Maximum Length:	27.05 m.
Stone Foundation Depth	229 mm	Maximum Width:	23.84 m.
Stone Above Chambers:	305 mm.	Approx. Bed Size Required:	621.51 square me- ters.
Average Cover Over Chambers:	458 mm.	System Compon	ents
Design Constraint Dimensions:	(50.00 m. x 27.50 m.)	<u> </u>	
		Amount Of Stone Required:	669 cubic meters
		Volume Of Excavation (Not Including Fill):	1042 cubic meters
		Total Non-woven Geotextile Required	:1702 square meters
		Woven Geotextile Required (excluding Isolator Row):	g 98 square meters
		Woven Geotextile Required (Isolator Row):	81 square meters
		Total Woven Geotextile Required:	179 square meters
		Impervious Liner Required:	0 square meters



UK and Ireland Office Locations

